

HANDEX OF MARYLAND, INC., 1350 Blair Drive, Suite H, Odenton, MD 21113

August 13, 1996

Mr. Steven Coladonato Project Engineer Sun Company, Inc. Ten Penn Center, 9th Floor 1801 Market Street Philadelphia, Pennsylvania 19103-1699

RE:

Short Pier Initial Investigation Report SUN Philadelphia Refinery

Pt. Breeze Processing Area

Dear Mr. Coladonato.

Handex of Maryland, Inc. is pleased to submit this Initial Investigation Report for the Short Pier area of the SUN Philadelphia Refinery, Pt. Breeze Processing Area. This investigation was conducted because product sheens have been detected on the water surface of the Schuylkill River near the Short Pier. This report presents the investigative methods and results, a recommendation for further investigation and interim product remediation, and a conceptual design for long term product remediation.

SUMMARY

A subsurface investigation was performed at the Short Pier in the South Yard of the Pt. Breeze Processing Area, because product sheens were detected on the Schuylkill River. The Short Pier is located along the river, and is constructed of a concrete and steel bulkhead and a subsurface wood decking. There are numerous product sources in the area.

In July 1996, six monitoring wells were installed and gauged, and product samples were collected for analysis. The well installation involved continuous split-spoon sampling. The subsurface geology consists of clay, silt, sand, and gravel indicative of fill material, underlain by a silty clay. Wood decking was located at two of the wells. Ground water flows to the west towards the river, with tidal fluctuations affecting the area within 50 feet of the river.

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Liquid phase and residual hydrocarbons were identified during the investigation. The liquid phase hydrocarbons were a mix of product types derived from the multiple product sources located to the east of the Short Pier. In addition, product may be migrating from the south along the river because the steel sheet piling impedes flow to the river. The product may be migrating into the river at openings in the bulkhead. In addition, product that accumulate in the void space below the decking may be released into the river during low tide when the river level is below the concrete facing. Product accumulates in the void space below the decking by seepage through the decking during low tide or by migrating on the water table east of the decking.

The remedial goal for the Short Pier is to prevent product from migrating into the Schuylkill River. This will require an additional investigation of the hydraulics in the area of the decking by installing a test trench to the top of the decking and determining the areal extent of the decking using ground penetrating radar (GPR). In the interim, product remediation at the Short Pier should include weekly bailing of product from the wells and recovery of any product detected in the test trench. Based on the current data, two conceptual remedial designs have been developed:

- Installation of a recovery well upgradient of the decking to capture the product prior to the decking area, and a trench type recovery system on top of the decking near the shoreline to prevent product migration into the river.
- 2. Installation of a hanging wall onto the concrete facing to retain product in the void space below the decking, and installation of a recovery system to remove the product retained below the decking.

AREA DESCRIPTION

The Short Pier is located along the eastern shore of the Schuylkill River in the South Yard of the Pt. Breeze Processing Area as shown on Figure 1. A detailed site plan of the Short Pier is presented as Figure 2. The Short Pier area is currently utilized for the transfer of product employing barges that dock south of the investigation area. The area between the river and the product (above and below ground) piping, and the area east of River Road are both relatively level. There is a moderate upward slope from west to east in the area of the above and below ground product piping.

The bulkhead along the river is constructed of either steel sheet piling which extends to the river bottom or a concrete facing that extends to a few feet above the river's low tide level. There is a wood decking at the Short Pier, although maps depicting the precise location are not available. A schematic of the decking in the area of the concrete facing, including approximate river levels, is shown on Figure 3. This shows the

The bulkhead along the river is concrete extends to the river bottom or a concrete river's low tide level. There is a wood decking the precise location are not available. A concrete facing, including approximate river concrete facing, including approximate river periods, not high tide.

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hydraulic connection between the river and the void space beneath the decking in the area where the concrete facing is present. The steel and concrete bulkheads meet at a notch that is not thoroughly sealed.

There are several product sources at the Short Pier area. Steel piping that transports product below the Schuylkill River emerges at the pipeline box (Figure 2). These pipes along with a numerous other product pipes are located above and below ground about 45 feet from the river. Additionally, there is a product processing area east of River Road, approximately 200 feet from the river.

INVESTIGATIVE METHODS

The initial investigation of the Short Pier area involved installation of six monitoring wells to determine hydrogeological conditions and evaluate for the presence and extent of product. Split-spoon samples were collected to evaluate the subsurface conditions. The investigation included gauging the wells for fluid levels and analysis of product samples collected from two wells.

Monitoring Well Installation

Six monitoring wells were installed at the Short Pier area on July 10 and 11, 1996, for subsurface hydrogeological and product data (Figure 2). Four wells (S-105 to S-108) are located along a line parallel to the Schuylkill River for evaluation of the area between the river and the product sources located to the east. Well S-109 is located about seven feet from the notch where the steel and concrete bulkheads connect. Product is suspected to be seeping into the river at this location; this area is referred to as the "seep" on Figure 2. The final well (S-110) is located at a sharp bend in the concrete wall that parallels the river along River Road. It is speculated that the wall, which extends at least 14 feet deep, serves as a barrier directing ground water and product parallel to the river until the bend in the wall where well S-110 is located. The wells were specified for installation to a total depth of ten feet below the water table. However, wells S-105 and S-109 were installed at shallower depths of 10 feet due to refusal on the wood decking at an elevation of approximately -2 feet.

The boreholes were drilled using hollow-stem augers operated from a mobile drill rig. The wells are constructed of 2-inch diameter, schedule 40, 0.020 slotted polyvinyl chloride (PVC) screen and 2-inch diameter, schedule 40, PVC casing. The annular space adjacent to the well screen was completed with #1 well gravel. The annular space above the well screen was sealed with hydrated granular bentonite. The remaining annulus was filled with a cement/bentonite grout. All of the wells were completed with a PVC stick-up and a protective casing, except S-109 which was completed flush to grade. Boring logs



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depicting well construction details are provided in Appendix A.

Soil samples were collected from the boreholes at wells S-105 through S-109 for geologic logging, hydrogeologic and product data, and possible grain size analysis. The sampling interval started at a depth of 5 feet and continued to the total depth of the borehole using a 2-foot long spilt-spoon sampler. Split-spoon samples could not be collected from well S-110, because of overhead utilities which prevented raising the drill rig mast. One or more soil samples were collected from each spilt-spoon and placed in a 16-ounce sealed glass jar. These samples have been retained and may be submitted for grain size analyses if the data is necessary for remedial design.

Product Sampling

Product samples were collected from wells S-109 and S-110 using a disposable, teflon bailer on July 15, 1996. The samples were submitted to the Philadelphia Refinery's on-site laboratory for API gravity and boiling point distillation analyses. The laboratory report is attached in Appendix B.

Monitoring Well Gauging

The depth to fluid in the six monitoring wells (S-105 through S-110) were gauged several times from July 11 through August 9, 1996. The data was collected using an audible electronic oil/water interface probe. On July 11 and August 8, the wells were gauged during consecutive high and low tides. The gauging data is presented on Table 1. The water table elevations for those wells with product are corrected using a specific gravity of 0.75.

INVESTIGATIVE RESULTS

The geologic conditions at the Short Pier consist of interbedded clay, silt, sand, and gravel (probably fill material), underlain by a silty clay. The wood decking was identified at two of the wells. Ground water occurs under water table conditions and flows west towards the river. The wells near the river are affected by tidal fluctuations. Liquid phase and soil residual hydrocarbons were identified in the wells at the Short Pier. The product migrates to the Short Pier area from the product sources located to the east. The pathways for the product to reach the river include openings in the bulkhead or access to the void space below the decking which drains into the river at low tide. Product reaches the void space below the decking by seepage through the decking or migration on the water table east of the decking.



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Geology

The subsurface geology was determined from the soil samples collected during well installation. Details regarding the geology at each well are presented on the boring logs (Appendix A). A geologic cross section parallel to the river (wells S-105 through S-108) is presented as Figure 4.

The geology in the area near the river is a mixture of clay, silt, sand, and gravel. The area has undergone significant construction disturbance, therefore much of the geology is probably fill material, although the precise depth of the fill material was not determined. The upper five to eight feet is a mixture of clay, silt, and sand that is indicative of fill material. This is underlain by sand and gravel with lesser interbedded clay to an elevation of -4 feet; this may also be fill material. The deepest layer identified is a silty clay with lesser interbedded sand that was logged to a an elevation of -9 feet. The exception to this silty clay layer is at well S-107 where coarse sediments (sand and gravel) continued to an elevation of -9 feet at which point the well was completed due to refusal on wood. None of the wells were installed beyond an elevation of -9 feet.

The subsurface wood decking was definitively identified at wells S-105 and S-109 at an elevation of approximately -2 feet. The wood decking was confirmed by at least two borings at each location and the elevation corresponded with the limited construction plans available for the area. A cross-sectional schematic of the decking is presented as Figure 4. Wood was also detected at well locations S-106, S-107, and S-108, but none of these cases were confirmed to be part of the wood decking. At well S-106, a 2-inch thick piece of wood was logged at an elevation of -3 feet, but the well was installed without refusal. Well S-107 was completed at an elevation of -9 feet due to wood refusal that may have been one of the stabilizing tie-backs; a second boring was not attempted. Wood was detected at well S-108 at an elevation of 0 feet; however, wood was not detected during the second boring.

The geology at well S-110 was not accurately identified, because neither splitspoon samples nor drill cuttings were available. According to the driller, the sediments from the surface to an elevation of 6 feet were loose and coarse indicative of fill material. The underlying material was also coarse, but seemed firmer.

Hydrogeology

Ground water at the Short Pier area is present as water table conditions in the unconsolidated sediments. Ground water flow is westerly toward the river. The topographically level area between the river and the product piping is impacted by the river's tidal fluctuations. The ground water gauging data is presented on Table 1.



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The ground water elevation in the wells near the river (S-105 through S-109) ranges from 2 to -2 feet, and fluctuates in correspondence to the tidal variability of the river. The tidal fluctuation in these wells varies from 0.6 to 2.2 feet, and may be greater because wells S-105 and S-109 are often dry at low tide. The tidal fluctuation for each well on August 8 is presented as Figure 5.

At well S-110, the ground water elevation is 13 feet; this well is not impacted by tidal fluctuations. The ground water elevation in well S-110 is slightly higher than the ground surface on the other side of the wall, where water was seeping through cracks at the bottom of this wall. Although not noted on Table 1, the ground water elevation in well S-110 is about 7 feet higher than at wells S-70 and S-71 (located abut 120 feet to the east). Several explanations are possible, including ground water mounding at well S-110 caused by the wall retarding ground water flow, perched ground water at well S-110/or an easterly ground water flow component (0.06 ft/ft gradient).

The river stage near well S-109 varied about 5 feet on August 8, from an elevation of -5.1 feet at low tide to an elevation of -0.1 feet at high tide. The low tide elevation was below the concrete facing of the bulkhead.

Ground water flow at the Short Pier area is generally to the west towards the river, with a slight southwestern component to the flow near the river. The ground water serves as a recharge source to the river during both high and low tides. The water table gradient is approximately 0.08 feet per foot (ft/ft) at high tide and 0.10 ft/ft at low tide. Contoured ground water elevation maps for high and low tide on August 8 are presented as Figures 6 & 7.

<u>Hydrocarbons</u>

Liquid phase and residual soil hydrocarbons were detected during well installation and well gauging. The liquid phase hydrocarbons were comprised of mixed product types from the are numerous product sources located hydraulically upgradient of the Short Pier area. The product migrates from the product sources to the east to the Short Pier along the westerly ground water flow direction. In addition, product may migrate to the Short Pier area from the south parallel to the river because the sheet piling impedes ground water and product flow into the river.

Based on the data collected and knowledge of the subsurface, the product seems to migrate into the river by two pathways. During high tide, product is detected on the water table above the wood decking as evidenced by well S-109. The product seeps into the river during high tide through openings in the steel or concrete facing. A seep has been visually detected at the contact between the steel and concrete bulkheads, because



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this contact is not completely sealed (noted as "seep" on Figure 2). Other seeps may be present, but have not been specifically identified.

As the river level recedes, the water level below the wood decking where the concrete bulkhead is present also recedes because it is hydraulically connected with the This creates a void space below the wood decking, where product may accumulate. When the river level recedes below the concrete facing, the product drains into the river. There are two possible pathways for the product to migrate into the void space below the decking:

- Product may seep through the decking. During low tide, the ground water elevation in well S-109 is at a similar elevation as the decking, therefore allowing the product to reach the decking. In turn, a void space within the decking or the void space below the decking may allow the product to drain from the well, evidenced by no product detected in the well S-109 at low tide.
- Product may migrate into the void space through the unconsolidated sediments east of the decking. This would require the ground water elevation east of the decking to be lower than the elevation of the decking. Because the location of the decking is uncertain, this pathway can not be confirmed.

Product has been detected in wells S-106, S-107, S-109, and S-110. The product data is presented in Table 1. A distribution map of the product thickness on August 8 at high and low tide is presented as Figure 8. The apparent product thickness in well S-106 has never been greater than 0.01 feet; residual hydrocarbons were detected during well installation from 0 to -5 feet.

At S-107, the maximum apparent product thickness was initially 0.01 feet (July 11-15), however, by August 8 the apparent product thickness reached a maximum of 1.56 feet. The product thickness in S-107 increases as the water level drops during low tide, indicative of product trapped between the soil pores. Residual hydrocarbons were detected during well installation at an elevation of -2 to -7 feet.

Product is consistently detected in well S-109 at high tide with an apparent product thickness of 0.41 to 1.87 feet. During low tide, the well is either dry (July 11) or product is not present in the well even though there is about 1 foot of water in the well (August 8 and 9). This is probably caused by the product draining into a highly porous void in the decking or the void below the decking. As the water level rises during high tide, the product is forced upward into the lower permeability material of the unconsolidated sediments, which forces the product to move into the well. Residual hydrocarbon were detected in the top eight inches of the wood, but were not detected in the formation.



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Product has been consistently detected in well S-110 at an apparent thickness ranging from less than 0.01 feet to 0.47 feet; this well is not affected by tidal fluctuations. The fluid level in this well is at a similar elevation as the product seeps detected at the bottom of the wall adjacent to the well.

Product has not been detected in wells S-105 and S-108; however, residual hydrocarbon were detected in well S-108 from an elevation of -2 to -4 feet. Although product has not been detected at wells S-70 and S-71 since December 1995, the screened interval of these wells is unknown, so the water table may be above the well screen which would prevent product from entering the well.

The product samples collected from wells S-109 and S-110 exhibited different types of product. The laboratory analytical data is presented in Appendix B. Well S-107 was not sampled because sufficient volumes of product were not detected in the well until August 8; a product sample will be collected in the near future. The API gravity for well S-109 was 38.4 degrees API as compared to 47.4 degrees API for the sample from S-110. The boiling point distillation curves are presented in graphical format on Figures 9a and 9b, and compared to the crude oil distillation curve. The product distribution for each sample are presented in Table 2. The product sample from well S-109 is a mixture of product types, whereas, the product sample from well S-110 is predominantly lighter end product types (gasoline and naphtha). The mixture of product types at well S-109 would be expected because it is located hydraulically downgradient of multiple product sources.

RECOMMENDATIONS

Further Investigation

The hydrogeologic system in the area of well S-109 requires additional investigation to determine the following:

- * The hydraulic connection between the unconsolidated sediments, the wood decking, and the void space below the decking
- The migration of product during low tide
- * The lateral and vertical extent of the product

A test trench located directly north of well S-109 and parallel to the river is recommended to visually evaluate the top of the decking. The trench will be approximately 2-feet wide by 6-8 feet long, and excavated to the top of the decking (approximately 10 feet deep). This trench can then be utilized for interim product recovery. Within the trench, ground water and product levels can be evaluated during tidal fluctuations, and the status of the product during low tide can be investigated. The



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areal extent of the wood deck will be investigated using ground penetrating radar (GPR) methodology.

Interim Remediation

In the interim, during which the further investigations will proceed, the following product remediation is suggested:

Manually bail product from wells S-107, S-109, and S-110 weekly

Recover product from the test trench using sorbents or a vacuum recovery truck

Future Remediation

The initial and proposed investigations will be evaluated to determine the most efficient and cost effective method to prevent product from reaching the Schuylkill River. Two possible remedial techniques are presented below as conceptual designs, with additional options possible based on the further investigations and the interim remediation results:

Option #1

- Analyze the soils from well S-107 for grain size to design a recovery well
- Install a recovery well at the location of well S-107
- Install a ground water pump in the recovery well to control product migration from the east towards the river
- Install a product pump in the recovery well to recover the product captured by the ground water cone of depression
- Install a product skimmer system in the test trench and recover the product using the following options: sorbent, vacuum truck, or pump

Option #2

- Install a hanging wall along the concrete bulkhead from the "seep" to the southern boundary of the pipeline box, and along the southern boundary of the pipeline box. The hanging wall would extend below the level of low tide to retain product in the void space below the decking.
- Create one or more apertures in the decking to allow the product to freely drain into this contained void space
- Install an automated oil mop at the fluctuating water surface below the decking to recover the retained product.

Option #2 will prevent product movement into the river more quickly than Option #1; however, installation of a hanging wall may be the most expensive task presented above.



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If you have any questions about this report of the project, please feel free to contact either of the undersigned at (410) 674-3200.

Sincerely,

urain M. Sahba

Senior Hydrogeologist

Glen Somes Director,

Industrial & Non-Retail Environmental

Services

AMS/GS:bw

Attachment

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FIGURES



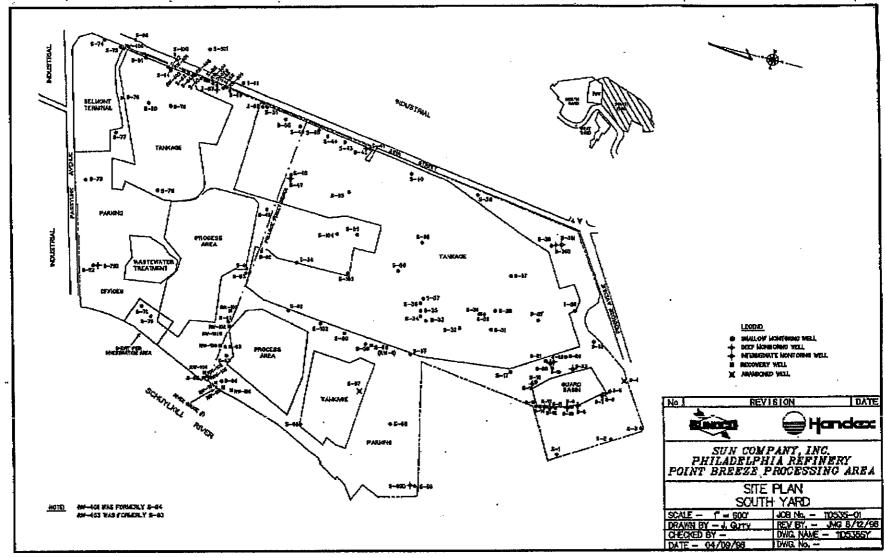
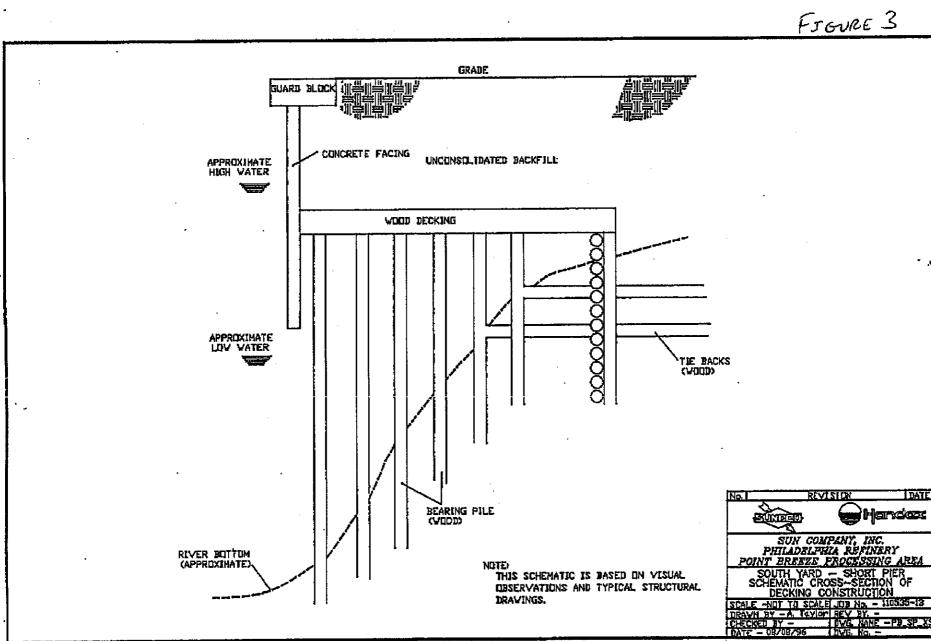
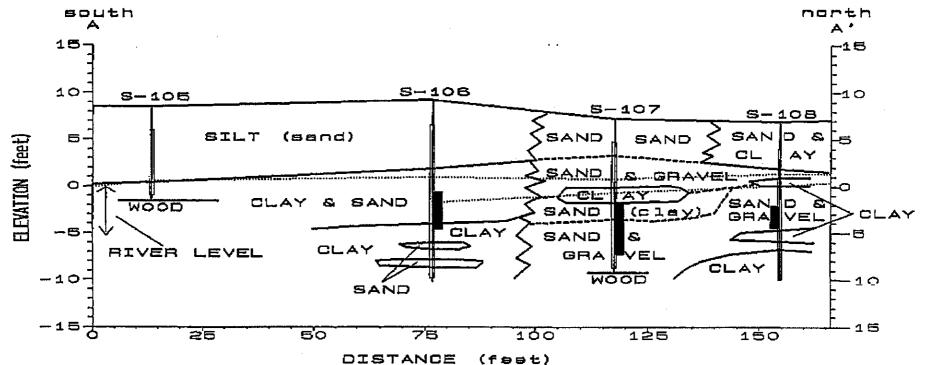


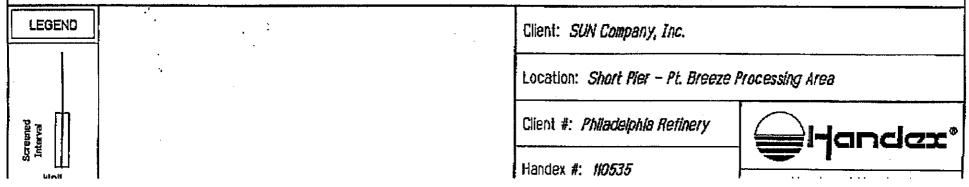
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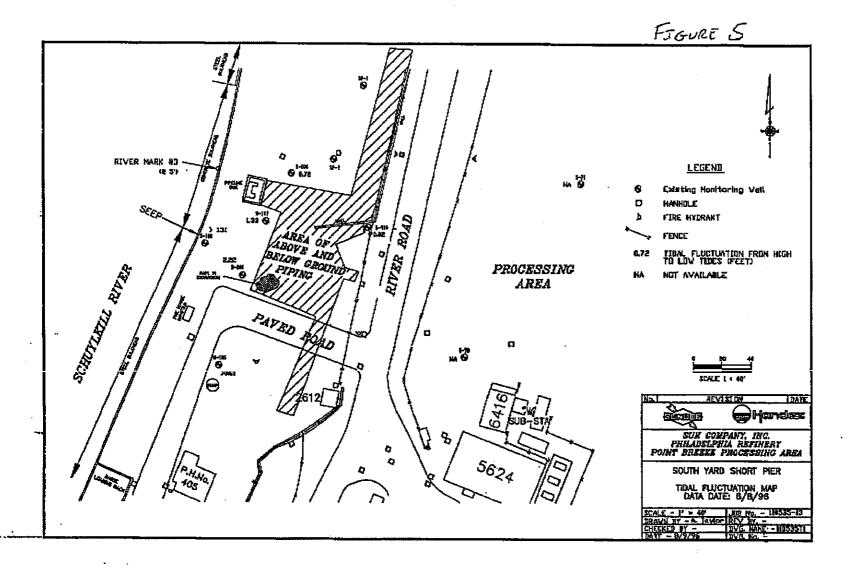


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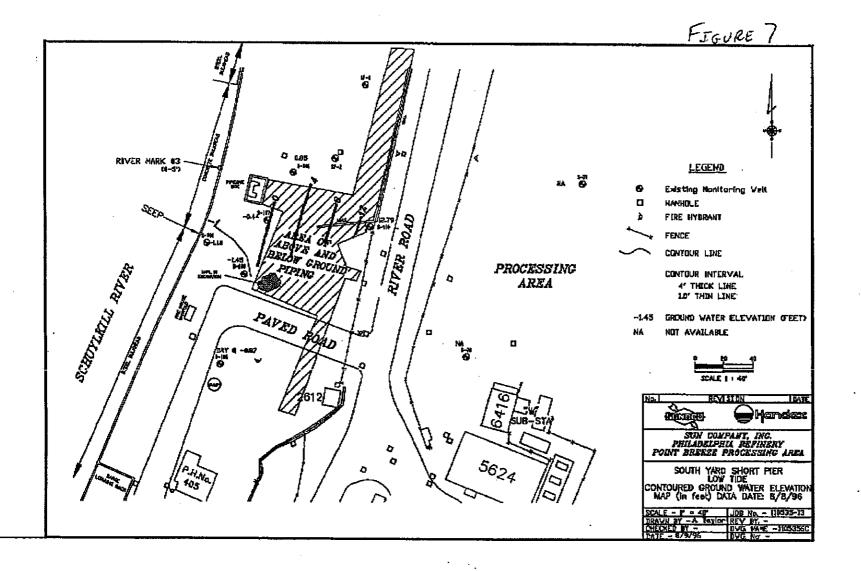


FIGURE 9a SUN PHILADELPHIA REFINERY SHORT PIER: S-109

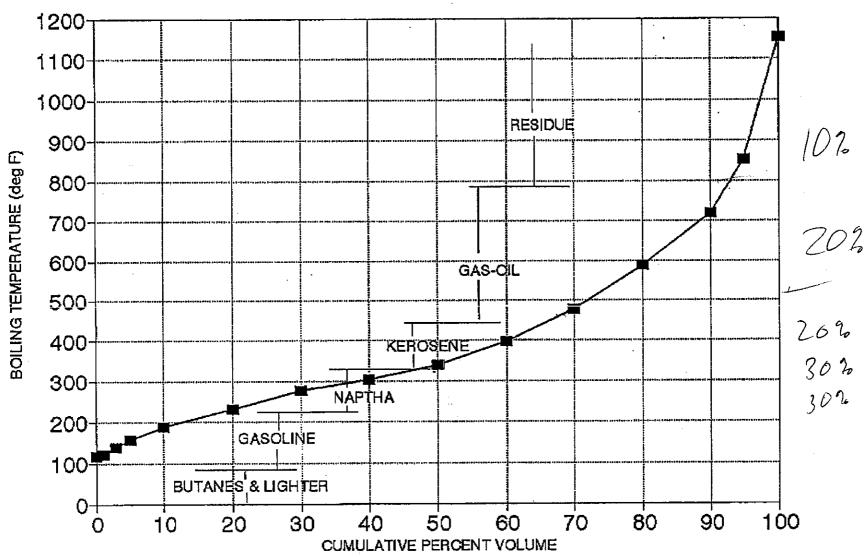
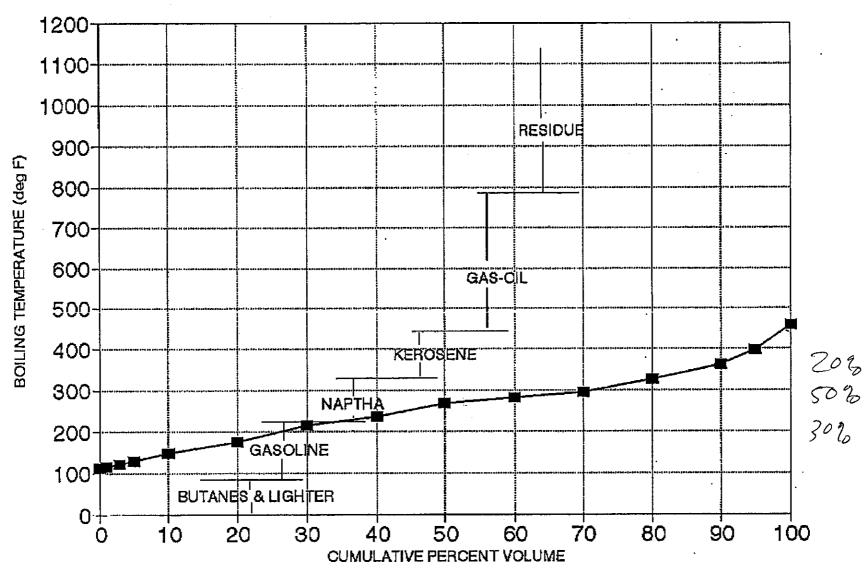


Figure 96 SUN PHILADELPHIA REFINERY SHORT PIER: S-110



TABLES



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GAUGING DATA

SUN - PHILADELPHIA REFINERY PT. BREEZE PROCESSING AREA

SOUTH YARD - SHORT PIER									
						•		CORRECTED	
			NAPL	WATER	NAPL	NAPL	WATER	WATER	}
	l		DEPTH	DEPTH	THICKNESS	ELEVATION	ELEVATION	ELEVATION	
DATE	WELL#	TIDE	(feel)	(feet)	(feet)	(feet)	(feet)	(feet)	COMMENTS
11-Jul-98	S-105	HIGH		10.54			0.14	0.14	
11-Jul-96	S-105	LOW		DRY			DRY	DRY	DRY @ -0.94 ft
12-Jul-96	8-105	HIGH.		10,35			0.32	0.32	
15-Jul-96	S-105	HIGH		10.14			0.54	0.54	
08-Aug-96	S-105	. HIGH		10,94			-0.26	-0.26	
08-Aug-96	S-105	LOW		DRY			DRY	DRY	DRY @ -0.87 ft
11-Júl-98	S-106	HIGH	10,95	10.95	<0.01	0.51	0.51	0.51	
11-Jul-96	\$-106	.LOW	12.93	12.93	<0.01	-1.47	-1.47	-1.A7	
12-Jul-96	\$-106	HIGH		10.83			0.63	0.63	
15-Jul-96	S-106	HIGH		10.29			1.17	1,17	, ,
08-Aug-96	S-106	HIGH	10,69	10.69	<0.01	0.77	0.77	0.77	
08-Aug-96	S-108	LOW	12.91	12.92	0.01	1,45	-1.48	-1.45	
11-Jul-96	S-107	HIGH	8.78	8.78	<0,01	0.68	0.68	0.68	
11-Jul-96	S-107	LOW	9.87	9.88	0,01	-0.41	-0.42	-0.41	
12-Jul-96	S-107	HIGH		8,71			0.76	0.75	
15~Jul-96	\$-107	HIGH		8.38		•	1.08	1.08	
08-Aug-96	S-107	HIGH	8.52	8.71	0.19	0.94	0.75	0.89	,
08-Aug-96	\$-107	LOW	9.51	11.07	1,56	-0.05	-1.61	-0.44	
11-Jul-96	S-108	HIGH		7.51			1.27	1.27	
11-Jul-96	S-108	LOW		8.20			0.68	0.68	
12-Jul-96	S-108	HIGH		7.53	, , , , , , , , , , , , , , , , , , ,		1.35	1.35	
15-Jul-96	S-108	HIGH		7.27			1.61	1.61	- ***
08-Aug-96	S-108	HIGH		7.31			1.57	1.57	
05-Aug-96	S-108	LOW		8.03			0.85	0,85	
11-Jul-96	S-109	HIGH	8.03	8.44	0.41	-0.62	-1.03	-0.72	
11-Jul-96	S-109	LOW		DRY			DRY	DRY	DAY @ -2.03 ft
12-Jul-98	S-109	HIGH	7.13	8.45	1,32	0.28	-1.04	-0.05	
15-Jul-96	S-109	HIGH	6.57	8.44	1.87	0.84	-1.03	0.37	
08-Aug-95	S-109	HIGH	6.90	8.12	1.22	0.51	-0.71	0.21	
08-Aug-96	S-109	LOW		8.51			-1.10	-1.10	
09-Aug-96	S-109	LOW		8.62	-		-1.21	-1.21	
11-Jul-96	8-110	HIGH	14.50	14.52	0.02	13,13	13.11	13.13	
11-Jul-96	S-110	LOW	14.50	14.50	<0.01	13.13	13.13	13.13	
12-Jul-96	S-110	HIGH	14.67	14,81	0.14	12,96	12.82	12.93	
15-Jul-96	S-110	HIGH	14.63	14.99	0,36	13.00	12,64	12.91	
08-Aug-98	\$-110	HIGH	14.74	15,21	0.47	12.59	12.42	12.77	·
08-Aug-96	5-110	LOW	14.74	15.16	0.42	12.89	12.47	12.79	
06-Aug-96	RIVER	HIGH		7,50			-0.10	-0.10	Approx. Value
08-Aug-96	RIVER	LOW		12.50	-		-5.10		Approx. Value
09-Aug-96	RIVER	LOW		12.40			-5.00		Approx. Value

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TABLE 2

SHORT PIER: CUMULATIVE PERCENTAGE OF PRODUCT TYPES BASED ON THE CRUDE OIL DISTILLATION CURVE

> **SUN - PHILADELPHIA REFINERY** PT. BREEZE PROCESSING AREA

PRODUCT TYPE	S-109	S-110		
Butanes & Lighter	0%	0%		
Gasoline	18%	35%		
Naphtha	28%	. 46%		
Kerosene	20%	17%		
Gas - Oil	26%	2%		
Residue	8%	0%		



APPENDIX A BORING LOGS



PAGE 27 (PRINTED PAGE 27)] 14:29 **23**9 410 674 3203 HANDEX MD HYDRO **2**1027 08/13/96 iandax WELL LOG: S-105 Handex Of Maryland Permit #: N/A Drill Date: July 10, 1998 Use: Monitoring Location: 3144 Passyunk Avenue, Philadelphia, PA Owner Loc #: Philadelphia Refinery Owner: Sun Company, Inc. Handex Loc #: 110535 BORING - Depth: 10 ft. Owner Address: Philadephia, PA Diameter: 8 in. Brilling Method: Hallow-Sten Auger CASING - Length: 4.75 ft. Diameter: 2 In. Sampling Method: Spilt Spoon SCREEN - Length: 7 ft. Diameter: 210. Static Water Level: 10.54 ft. (July 11, 1996) WELL - Depth: 9.75 ft. Depth Graphic Log Jepth (11.) Well Diagram 30M3/8 Sample Geologic Description Protective Casing 2 PVC Salick-Up Tan to light orange SILT, some fine Sand (wet 86.5") Sand Cement Bentonite 105-1 3-3-2-2 Ю5-2 2-1-1-2 Black CLAY, and line to coarse SAND, trace fine to medium Gravel (moist to wet: clay as IO5-3 1-2-2-38 matrix and nodules; gravel angular; slight organic odor; strong hydrocarbon odor and 10 stain at 10.0'-10.5') WOOD (Top I/3 was wet and steined with hydrocarbons; bottom 2/3 was dry and clean; horizontal layering) NOTE: A second boring was drilled 3 feet northwest due to the refusal on the wood. A sample was

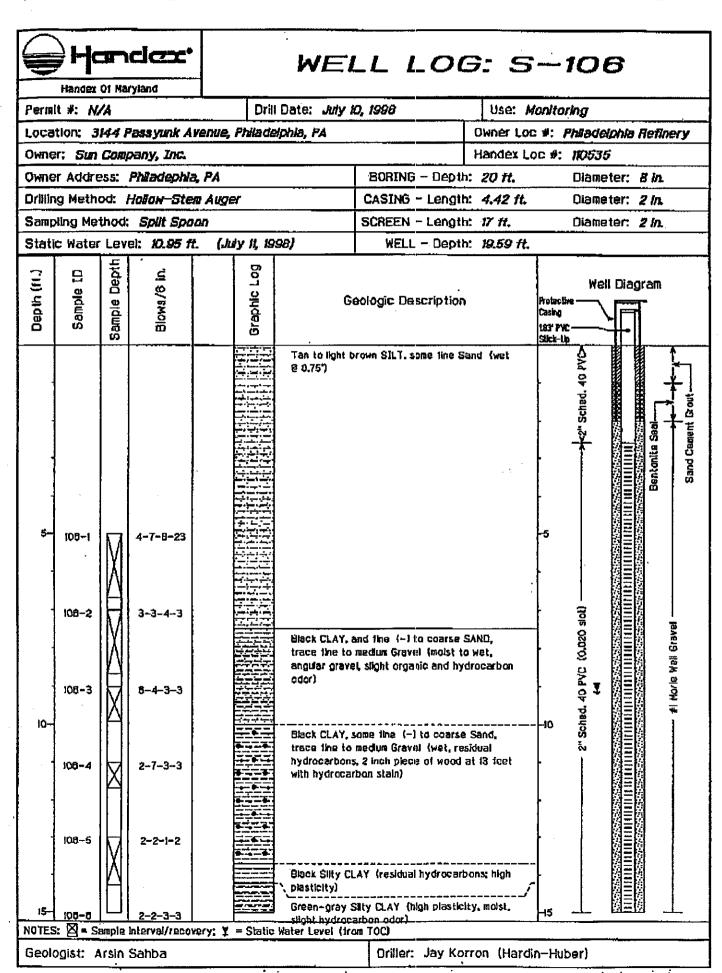
collected from 10-12 foot interval (blow counts: i-2-35/3). The spoon refused on wood at it feet. The wood was similar to the first boring, except layering was diagonal (45 degrees). The well was installed in the second boring. 60

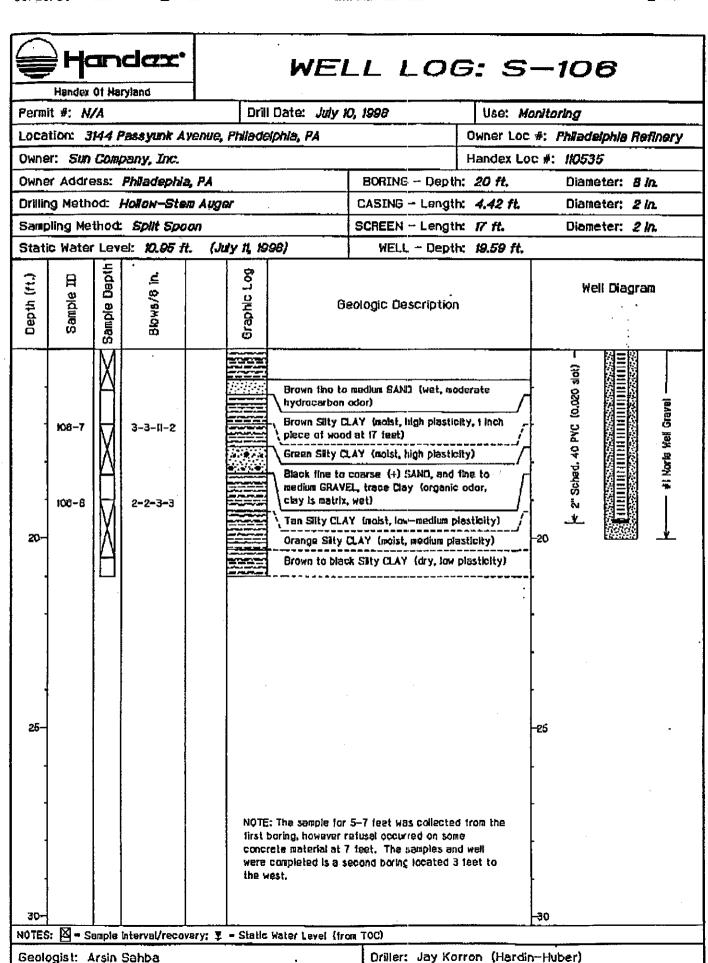
NOTES:

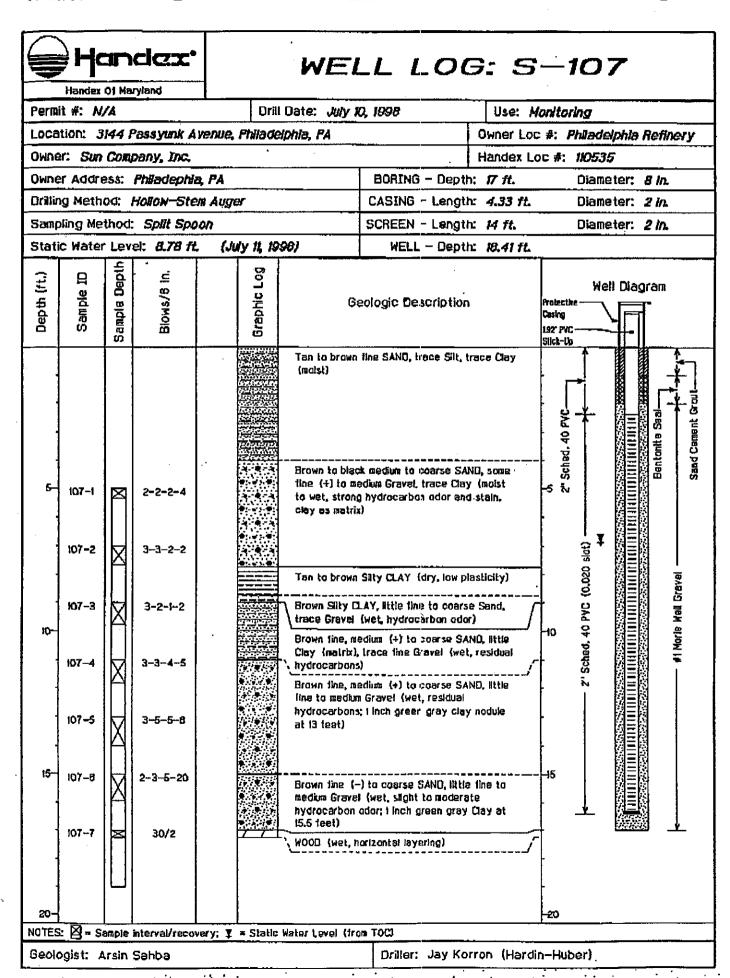
= Sample interval/recovery: ▼ = Static Water Level (from TOC)

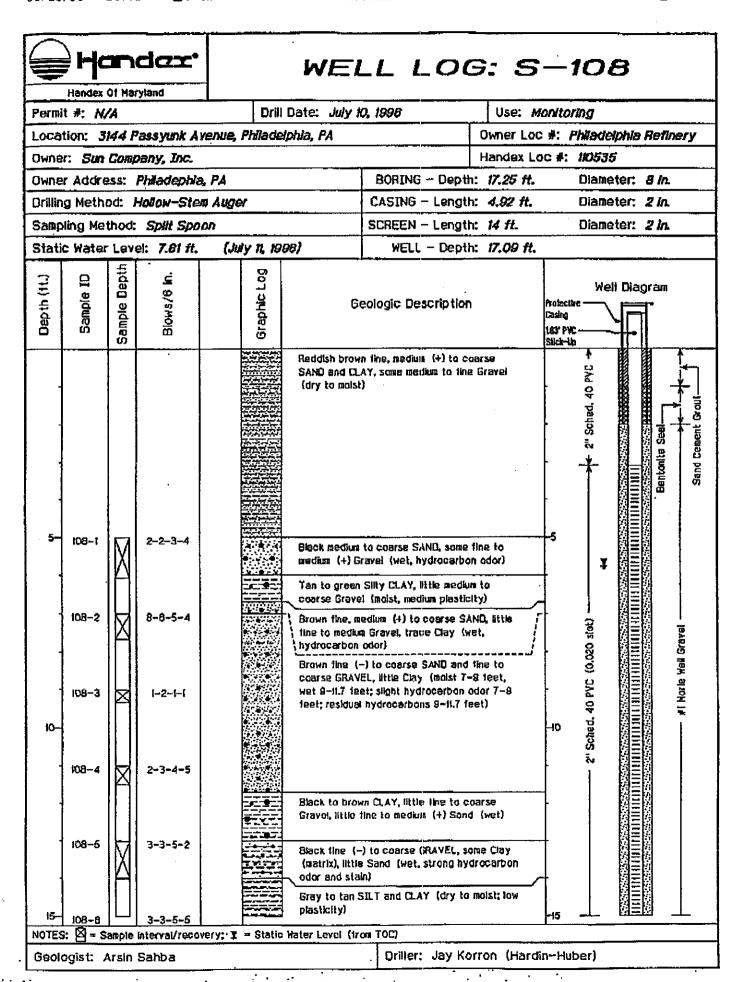
15

Geologist: Arsin Sanba Driller: Jay Korron (Hardin-Huber)

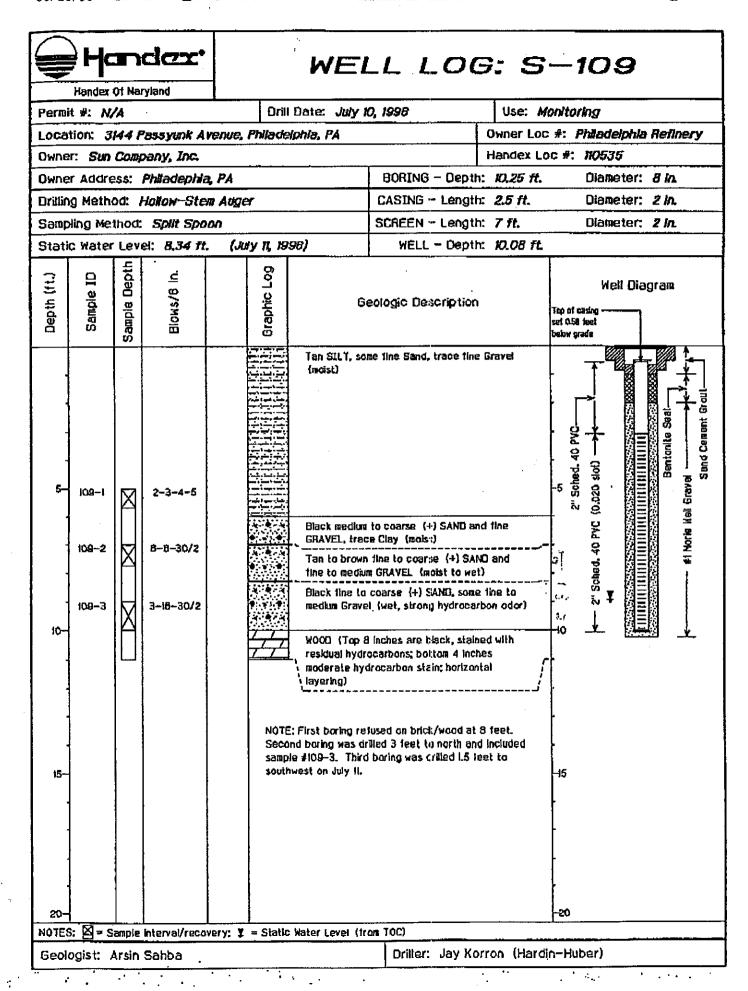








				<u> </u>							
Handex Of Naryland				_	WELL LOG: S-108						
Permit #: N/A					Drill Date: <i>July 10, 1996</i>				Use: Manitaring		
	·		assyunk A	venue,	Philadelphia, PA			Owner Loc #: Philadelphia Refinery			
			pany, Inc.			<u>· </u>			c #: <i>110535</i>		
			Philadephia	9, <i>PA</i>			BORING - Depth	: 17.25 ft.	Diameter: 8 in.		
		-	Hollow-Ste				CASING - Lengtl	1: 4.92 ft.	Diameter: 2 In.		
Samp	ling Me	thod:	Split Spa	on			SCREEN - Lengti	n: <i>14 ft</i> .	Diameter: 2 In.		
Stati	c Water	Lev	el: <i>7.61 ft</i> .	(JL	iy 11, 19	98)	WELL - Depti	n: <i>17.09 ft</i> .			
Depth (f1.)	Sample 1D	Sample Depth	Blows/6 In.		Graphic Log	G	eologic Description	,	Well Diagram		
20-	108-7		3-3-4-3		3 tec	plasticity) Brown Silty C plasticity) E: First boring rei	w Silty CLAY (moist; high size of the medium second boring a through 1061~7 and the	i. Naved	2" Schad. 40 PVC (0.020 slot)		
30-	: ⊠= S	ample	interval/reco	very; ‡	■ Static	Water Level (1re	om TOE)		-30		
Geole	ogist: A	Irsin	Sahba		_		Driller: Jay Ko	rron (Hardi	n-Huber)		



[RECEIVED 08/13 16:25 1996 AT 2152468313 PAGE 34 (PRINTED PAGE 34)] 08/13/96 14:33 \$\mathbb{T}\$ 410 674 3203 HANDEX NO HYDRO

	<u> </u>			-		WE	LL LO	G: S	;—110	
Handex Of Naryland Permit #: N/A				J	Drill Date: July 11, 1998			Use: Manitaring		
			ssyunk Av						#: Philadelphia Refinery	
			any, Inc.	C110C3 .	/ #9710	ijanoj . A			oc #: <i>110535</i>	
		-	hiladephia,				BORING - Depti	<u> </u>	Diameter: 8 In.	
			ollow-Stea				CASING - Lengti		Diameter: 2 in.	
	ng Meth						SCREEN - Lengti		Diameter: 2 in.	
			: 14.51 ft.		iy 11, 19:	 .gg}	WELL - Depti			
					· ·	· · ·				
Depth (ft.)	Sample ID	Sample Depth	Blows/8 In.		Graphic Log	G r	eologic Description))	Protective Casing 2.42 PVC Stick-Up	
15-						gravel and ru	S. Loose sediments including Possible Passible Packting S. Sediments tirmer that Less grayel, no rubble.	an 0–22	2" Sched. 40 PVC 10.020 slat)	
30~				:		because the to overhead	spoon samples were not drill rig could not be ra utilities. Residual hydro ed on the bottom 20 fe	aksed due ocarbons	-30 -35	

APPENDIX B
PRODUCT ANALYTICAL DATA



PAGE 36 (PRINTED PAGE 36) 1 [RECEIVED 08/13 16:26 1996 AT 2152468313 HANDEX MD HYDRO 08/13/96 14:34 **23**9 410 674 3203

2036 7:40 No.002 P.02

TECH.SVCS.

TEL:1-215-339-7547

Aug 06,95

Sample JD: 200244913 User Sample JD: SPCL SHORT PIER 5109

Date Loggest: 08/05/96 10:13 Sample Type: KYKXXX UNDEFINED PRODUCT Material Neme: MISC. UNDEFINED PRODUCT

Tag Date: Assoc'd ID:

Material Type: PLANT SAMPLE

Status: COMPLETE

Condition: APPROVED

Comments; Old SAMPLES FROM WEL Batch:

Component	<u>Units</u>	Result	MinSpec NaxSpec
********			******
API GRAVITY	deg AP1	38.4	
INITIAL BOILING POINT (GC)	deg: F	117	
01 X (GC)	deg F	121	
03 % (GC)	deg F	140	
05 % (BC)	deg F	157	
10 % (GC) .	deg F	189	
50 X (BC)	dég ?	231	
30 % (GC)	deg F	277	
€0 X:(GC)	dog f	305	
50 % (GC)	dog F	341	
40 % (GC)	deg 7	298	
70 ¥ (GC)	deg f	479	
80 % (GC)	deg F	588	
90 % (GC)	deg F	720	
95 % (CC)	dog f	853	
FND POINT (CC)	dea F	1154	

PAGE 37 (PRINTED PAGE 37)] 08/13/96 14:34 279 410 674 3203 HANDEX MD HYDRO

Ø037

TECH.SVCS.

TEL:1-215-339-7547

Aug 06,96

7:40 No.002 P.03

Sample ID: 200244915 User Sample ID: SPCL SHORT PIER \$110

Date Loggad: 08/05/96 10:18

Sample Type: XXXXXX UNDEFINED PRODUCT

Yes Date:

Material Name: MISC. UNDEFINED PRODUCT

Accec'd ID:

Natorial Type: PLANT SAMPLE

Status: COMPLETE

Conditions APPROVED

Comments: Dit SAMPLE FROM WELL Batch:

Coopenent	Unite	Result	MinSpec MaxSpec
		40000	
API GRAVITY	deg AP1	47.5	•
INITIAL BOILING POINT (GC)	deg F	113	
01 % (EC)	deg f	114	
OF X (\$C)	deg F	122	
05 X (GC)	deg F	129	
10 % (60)	deg F	148	
20 % (OC)	deg F	174	
30 % (QC)	deg F	216	
40 % (8C)	dag F	235	
50 X (GE)	dog F	268	
60 % (ec)	depf	283	
70 X (GC)	deg F	295	
80 % (GC)	dog F	327	
99 X (GC)	deg F	363	
95 % (GC)	deg F	399	
END POINT (QC)	deg F	458	