REPORT

GEOTECHNICAL INVESTIGATION DELOACH AND SHORT WHARVES REPAIR

SUNOCO PHILADELPHIA REFINERY PHILADELPHIA, PENNSYLVANIA

Prepared for Sunoco, Inc. (R&M) 3144 Passyunk Avenue Philadelphia, PA 19145

January 10, 2012



URS Corporation 335 Commerce Drive Suite 300 Fort Washington, PA 19034 215.367.2500

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January 10, 2012 19998935.00001

Ms. Jane Chen, PMP Sunoco, Inc. 3144 Passyunk Avenue Philadelphia, PA 19145

Subject: Report on Geotechnical Investigation Proposed Deloach and Short Wharves Repair Project Sunoco Philadelphia Refinery Philadelphia, Pennsylvania

Dear Ms. Chen:

We are pleased to present herein our report of a geotechnical investigation which was performed in connection with the proposed Deloach and Short Wharves Repair Project at the Sunoco Philadelphia Refinery in Philadelphia, Pennsylvania. This investigation was performed in accordance with our proposal dated March 4, 2011, and Sunoco SPO No. 11-PT2087, dated June 21, 2011.

Soil samples which were obtained during the investigation will be retained in our laboratory for a period of three months, after which they will be returned to you for proper disposal.

We sincerely appreciate the opportunity to be of service to you on this project. If you have any questions on the contents of this report, or if we may be of additional service, please give us a call.

Very truly yours,

Jetti

Yongli Min, P.E. Principal Engineer/Project Manager

John C Valh

John C. Volk, P.E. Vice President/Geotechnical Engineering Manager

cc: Neil Scafonas, URS

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Appendix B Laboratory Testing

The Geotechnical Investigation reported herein was performed at the request of Sunoco, Inc. (Sunoco), in connection with the proposed Deloach and Short Wharves Repair project at the existing Sunoco Philadelphia Refinery in Philadelphia, Pennsylvania. The project location is shown on Plate 1, Regional Location Plan.

The purpose of this investigation was to evaluate the geotechnical conditions of the site and to formulate conclusions and recommendations pertaining to the design and construction of the proposed repairs. Our services consisted of planning the investigation, full-time monitoring of the subsurface exploration program consisting of test borings, laboratory testing of representative soil samples, engineering analysis of the data obtained, and preparation of this report.

A description of the subsurface exploration program and test boring logs are presented in Appendix A. The geotechnical laboratory testing program is described and the results are summarized in Appendix B. Relevant findings, conclusions, and recommendations derived from this investigation are presented in the following sections.

Based on the information from Urban Engineers, Inc. (UEI), the project designer, the proposed repair work may consist of replacing existing bulkhead with a combination of sheetpiles, soldier piles, anchoring systems consisting of concrete deadman or anchoring piles, placing stone riprap, strengthening existing sheet piles, installing new sheet piles and new lateral support structures.

The Deloach and Short Wharfs are a part of the South Yard Terminal which is located on the Schuylkill River, approximately 3¹/₄ miles upriver of the confluence with the Delaware River and approximately ¹/₄ mile downriver of the Passyunk Avenue Bridge, in Philadelphia, Pennsylvania, as shown in Plate 1 and Plate 2.

The South Yard Terminal is an approximately 1050 feet long wharf, consisting of a continuous anchored steel sheet pile bulkhead and is separated into two designated berths, the Short Wharf and Deloach Wharf. The Short Wharf and Deloach Wharf are situated on the upriver portion of the terminal and measure approximately 450 feet long each. The Pollock Street sewage outfall structure and water intake structures are located at approximately 150 feet of the downriver portion of the terminal A deck structure, without an outshore bulkhead fascia exists at the upriver end of the South Yard (beyond the 1050 feet length). The South Yard functions as a berth for marine vessels, typically barges, for the loading and unloading of various petroleum based products.

The original construction of the wharves at the South Yard Terminal varies along its length. From Station 0+00 to approximately Station 1+05, the original wharf consisted of a timber pile supported low level timber deck wharf structure with timber sheeting cut-off wall. From Station 1+05 to Station 9+00, the original wharf consisted of a steel HP-pile supported low level concrete deck with a steel sheet pile cut off wall. Both types of wharf structures support a concrete seawall retaining approximately 8 to 12 feet of fill material. The date of the original construction of these wharf structures is not known. Circa 1980, the terminal structure was modified with a continuous tied-back steel sheet pile bulkhead installed along the outshore face of the wharf. The steel sheet pile bulkhead wall was anchored using anchors located inshore of the face of the bulkhead. The anchor construction varies from steel sheet pile wall, to steel batter pile supported reinforced concrete block, to reinforced concrete deadman along the length of the terminal. The steel sheet pile bulkhead is protected by a timber fender system consisting of timber fender piles spaced at approximately 10 feet 3 inches on centers along the length of the bulkhead. The timber fender piles are attached to the steel sheet piling with chain and pad eye connections. Located between the fender piles and steel sheet piling are two timber chocks and a square rubber fender.

From Station 9+00 to Station 10+50, the original wharf appears to be a steel sheet pile bulkhead with battered steel HP-pile anchors driven through penetrations in the steel sheets and connected directly to the bulkhead. This area had previously supported a boat launch gantry crane system, which was removed due to a bulkhead failure circa 1996.

The existing grade slopes gently downward towards the river and towards south. The elevations of the existing grades are not available as of this writing. The elevation values reported here are based on field measurements by URS, assuming the top of concrete at the northwest corner of the warehouse building to be at El. 100 ft.

A review of available geologic information indicates that the site is underlain by fine-grained alluvial deposits which are underlain by the granular alluvial soils of the Trenton Gravel. The Trenton Gravel formation generally consists of gravelly sand and interbedded sand and clay-silt layers. The bedrock at the site consists of mica schist and gneiss of the Wissahickon Formation. Within the refinery, there is generally a layer of man-made fill over the natural deposits.

The subsurface conditions at the site were explored by means of nine test borings, six of them behind the bulkhead on land and three immediately in front of it in the river. The number and locations of the borings were recommended by UEI. The locations of test borings are shown on Plate 2, Site and Boring Location Plan. The borings were drilled to depths ranging from approximately 80 to 98 feet below the existing grades behind the bulkheads. Logs of the test borings are presented in Appendix A, together with a description of drilling and sampling methods. Geotechnical laboratory test results are presented in Appendix B. Inferred subsurface profiles are shown on Plates 3 through 5. The various strata encountered are described below.

4.1 STRATUM 1 – FILL

The fill stratum was encountered below the ground surface in all borings except Borings B-4 and B-7.

In the three water borings (B-1, B-4, and B-7), the fill was only encountered in Boring B-1 below the mud line, consisting of silty clay with concrete fragments and wood, with a thickness of approximately 9 ft. The standard penetration test (SPT) N-values vary from weight of rods (WOR) to 30 blows per foot (bpf), indicating an erratic density condition.

Significant amount of fill was encountered in the three borings behind the bulkhead (B-2, B-5, and B-8) with a thickness varying between 32 ft in Boring B-2 and 53 ft in Boring B-8. The fill consist of silty coarse to fine sand and gravel on the top, grading into silty medium to fine sand with occasional concrete and brick fragments, and wood. The SPT N-values ranged between 2 to 52 bpf. Typically, the top of the fill stratum is judged to be in a dense condition, and the lower portion of the fill in a loose to medium dense condition.

The fill was also encountered in the three land borings (Borings B-3, B-6, and B-9) with a thickness of approximately 5 to 13 ft, consisting of silty coarse to fine sand and gravel with brick and concrete fragments. Based on the resistance encountered during utility clearing using vacuum extraction method (hydro-excavation), the fill in these three borings is judged to be in a dense condition.

Results of five moisture content tests indicate a moisture content of 14 to 33 percent, averaging 24 percent. Grain-size distribution curves on selected fill samples are shown in Appendix B.

Corrosivity testing on one sample indicates pH value of 7.8, resistivity of 8,200 Ω -cm, and no detectable chloride, sulfate, and sulfide.

Organic vapor concentration of soil samples varies from 14 to over 10,000 parts per million (ppm). The highest reading was recorded in Borings B-3 and B-8.

4.2 STRATUM 2 – UPPER CLAY

This stratum was encountered right below Stratum 1 in Borings B-6 and B-9 with a thickness of approximately 4 and 12 ft. The soils consist of gray fine sandy silty clay. The SPT N-value was 2 bpf. Based on the resistance encountered hydro-excavation, the soils are judged to be firm to stiff condition.

Results of one moisture content test indicate a moisture content of 24 percent. The grain size distribution curve is shown in Appendix B. Results of an Atterberg limit test indicate a liquid limit of 24 percent and a plastic limit of 15 percent.

Organic vapor concentration of soil samples varies from 340 to 800 ppm.

4.3 STRATUM 3 – UPPER SAND AND GRAVEL

This stratum was encountered in Borings B-3, B-6, and B-9 below Stratum 1 or Stratum 2, with a thickness of approximately 5 to 9 ft. The soils consist of gray coarse to fine sand and gravel with trace silt. The SPT N-values range from 23 to 52 bpf, averaging 33 bpf, indicative of a medium dense to dense condition.

Results of one moisture content test indicate a moisture content of 9 percent. The grain size distribution curve is shown in Appendix B.

No organic vapor concentration was detected in the soil samples in this stratum.

4.4 STRATUM 4 – LOWER CLAY

This stratum was encountered below Stratum 1 and Stratum 3 in Borings B-3 through B-6, and B-9. The soils consist of gray sandy silty clay to sandy silt. The thickness of this stratum is approximately 1 ft in Boring B-4, and 12 to 21 ft in other borings. The SPT N-values range from 2 to 20 bpf. The Pocket Penetrometer Resistance (PPR) values typically vary from 0.5 to 1.5 tsf, indicative of a firm to stiff consistency.

Results of moisture content tests indicate that the moisture contents ranged from 24 to 37 percent, averaging 30 percent. Grain size distribution curves are shown in Appendix B. Results of five Atterberg limit tests indicate liquid limits ranging from 24 to 46 percent and plastic limits from 20 to 27 percent.

Three unconsolidated-undrained (UU) triaxial compression tests indicate undrained shear strengths of 500 to 1,700 psf, averaging 1,200 psf, indicative of a firm to stiff consistency. Two consolidation tests indicate preconsolidation pressure of approximately 4 tsf and 5.6 tsf, with compression ratios of 0.19 and 0.17, and recompression ratios of 0.025 and 0.015 (all strain based).

No organic vapor concentration was detected in the soil samples in this stratum.

4.5 STRATUM 5 – LOWER SAND AND GRAVEL

This stratum was encountered beneath Stratum 1 or Stratum 4 in all borings, extending to a depth of approximately 79 to 87 ft below grade. The soils consist of brown medium to fine sand on the top of this stratum, grading into gray and brown silty coarse to fine sand with varying amounts of gravel. SPT N-values range from 7 to 113 bpf. The top portion of the stratum is judged to be in a medium dense condition, and lower portion in a dense to very dense condition.

There are layers of interbeded clay within this stratum, which is described in detail in Section 4.6.

Results of moisture content tests indicate that the moisture contents ranged from 4 to 23 percent, averaging 11 percent. Grain size distribution curves are shown in Appendix B.

No organic vapor concentration was detected in the soil samples in this stratum.

4.6 STRATUM 5A – INTERBEDDED CLAY

This stratum was encountered within Stratum 5. The thickness of the layers ranges from approximately 1 ft to 18.5 ft. Typically, the top of the layer is encountered below a depth of 60 ft. The soils consist of gray clay with thin partings (less than 1/32 inch in thickness) of very fine sand. SPT values of the soils range from 11 to 47 bpf, averaging 25 bpf. The PPR values vary from 1 to 3 tsf, indicative of a stiff to very stiff consistency.

Results of moisture content tests indicate that the moisture contents ranged from 8 to 44 percent. Grain size distribution curves are shown in Appendix B.

No organic vapor concentration was detected in the soil samples in this stratum.

4.7 STRATUM 6 – DECOMPOSED ROCK

This stratum was encountered beneath Stratum 5 or 5A in all borings. This stratum was not fully penetrated in all borings except Borings B-3 and B-9 with a thickness of 4.5 to 6 ft. The decomposed rock consisted of light gray micaceous silty course to fine sand and gravel-size rock fragments. Relict rock structure was apparent in the soil samples. The SPT values are more than 50 bpf, indicative of a very dense condition.

4.8 STRATUM 7 – BEDROCK

The bedrock was cored in two test borings, B-3 and B-9, with a core length of 5 feet each. The bedrock consists of moderately weathered mica schist. The core runs had a recovery of 75 and 52 percent, and the Rock Quality Designation (RQD) of 12 and 13 percent.

4.9 GROUNDWATER

As a part of the investigation, groundwater monitoring well were installed in Borings B-2, B-3, B-5, B-6, B-8, and B-9. The groundwater readings are tabulated in each boring log. The groundwater was observed to be at 7 to 12 ft below grade, corresponding to El. 94 to El. 104 during the field investigation in August 2011. Higher elevations were observed in the borings in the northern portion of the site (B-8 and B-9). It should be noted that groundwater levels are subject to seasonal and long-term variations due to tidal, climatic, and man-made influences.

The subsurface of the project site consists of six different soils strata as described in Section 4. From land side to the river, the soil stratigraphy above Stratum 5 soils change drastically, as the fill thickness increases significantly towards the river. This is illustrated by the three inferred subsurface profiles (Plates 3, 4, and 5).

Per our discussion with UEI, the proposed repair will likely consist of new sheetpiles and soldier piles in the front of the bulkhead, and anchors on the land side to provide lateral support. The anchors could consist of either concrete deadman or battered driven piles, or a combination of both. The piles that are being considered are HP12x53, HP12x74, HP14x73, and 14-inch and 16-inch outside-diameter (OD) open-end steel pipe piles with ½-inch wall thickness. Due to the presence of dense sand and gravel, HP12x53 piles may be too light to penetrate through in order to derive the required tension capacity. The design recommendations are provided in Section 6.

Recommendations pertaining to the design and construction of foundations and earthworks for the proposed repairs are presented below.

6.1 FOUNDATIONS

6.1.1 Design Soil Parameters

The following design soil parameters should be used for the design of the anchor structures:

Items	Stratum 1 Fill	Stratum 2 Upper Clay	Stratum 3 S&G	Stratum 4 Lower Clay	Stratum 5 S&G	Stratum 5A Stiff Clay	Stratum 6 Decomposed Bedrock		
Total Unit Weight (pcf)	120	110	125	115	125	120	130		
Buoyant Unit Weight (pcf) ⁽¹⁾	58	48	63	53	63	58	68		
Internal Friction Angle (°)	30	0	32	0	32	0	35		
Cohesion (psf)	0	500	0	750	0	1,500	0		
Active Earth Pressure Coefficient, K _a	0.33	0.5	0.31	0.5	0.31	0.5	0.27		
Passive Earth Pressure Coefficient, K _p	4.5	2.5	5.5	2.5	5.5	3.5	6.0		
Concrete to Soil Coefficient of Friction	0.35	0.3	N.A.	N.A.	N.A.	N.A.	N.A.		
<u>LPILE</u> Soil Type	Sand	Soft Clay	Sand	Clay	Sand	Stiff Clay	Sand		
<u>LPILE</u> ε_{50}	N.A.	0.02	N.A.	0.01	N.A.	0.005	N.A.		
LPILE Soil Modulus, k (pounds per cubic inch)	40	50	120	100	120	200	200		

Table 1 – Foundation Design Parameters

6.1.2 Pile Foundations

Design: It is understood that the piles to be used may consist of HP 12x74, HP14x73, and 14inch and 16-inch OD open-end pipe piles with $\frac{1}{2}$ inch walls. The piles should have a minimum yield stress of 36 ksi and meeting requirements of ASTM A36 or A572 steel. All welds (e.g., splices) in the pile should be full-penetration butt welds conforming to the current edition of the Structural Welding Code, D1.1, American Welding Society.

The following design capacities may be used. The tension capacity requires a minimum length of 80 ft below the grade behind the bulkhead.

Pile Type	HP12x74	HP14x73	14-inch OD Open-end Pipe	16-inch OD Open-end Pipe
Allowable Capacity – Compression (tons)	80	90	80	95
Allowable Capacity – Tension (tons)	40	45	40	45

Table 1 – Pile Design Parameters - Piles on Landside

Table 2 – Pile Design Parameters - Piles on Waterside

Pile Type	HP12x74	HP14x73	14-inch OD Open-end Pipe	16-inch OD Open-end Pipe
Allowable Capacity – Compression (tons)	40	40	40	40
Allowable Capacity – Tension (tons)	10	10	10	12

The allowable compression and tension capacities of the pile may be increased by 33 percent for short term loading due to wind and earthquake.

Construction: All piles are expected to be seated into the decomposed rock of Stratum 6 to derive the design capacities. The contractor shall select a hammer capable of delivering sufficient energy to pile tips while not exceeding practical refusal for the hammer and while not exceeding 90 percent of the yield stress of the pile during driving. The Contractor should submit pile hammer and wave equation analysis for the Geotechnical Engineer (URS) to review prior to starting work. The piles are expected to be driven to a depth of approximately 80 feet below the grade behind the bulkhead to derive the required capacities.

All piles should be installed within 3 inches of design location and should not be more than 2 percent out of plumb. Piles should not be collapsed, bent, or otherwise damaged. Any non-conforming piles should be replaced by the contractor at no cost to the owner.

If obstructions are encountered prior to reaching terminal resistance, the pile should be withdrawn or abandoned and a replacement pile driven. In that event, the structural engineer should determine the location of replacement or additional piles and determine if a redesign of the pile cap is required.

Dynamic pile load tests using a Pile Driving Analyzer (PDA) should be used on at least three piles. The PDA tests should confirm a mobilized capacity of at least 2.5 times the design capacities of the pile, as indicated above.

6.2 SEISMIC CRITERIA

Based on the 2009 International Building Code (IBC), Site Class D is recommended.

6.3 STRUCTURAL FILL

Structural fill may be required below and around the anchors, and for replacement of unsuitable materials under loaded areas. All structural fill should be placed and compacted in accordance with the following recommendations.

Materials to be used for structural fill should be well-graded, predominantly granular, and free from roots, vegetation, organic material, trash, wood, or other deleterious matters. The granular portion of the fill may be used as structural fill around the footings and other loaded areas. Below the planes of new foundations, the structural fill should consist of material conforming to the requirements of "Selected Structural Fill" which is defined as Penn DOT Coarse Aggregate No. 2A.

All structural fill should be placed in essentially horizontal lifts, not more than 8 inches in loose thickness. Structural fill for support of foundations should be compacted to not less than 95 percent of the maximum "modified" dry density as defined by ASTM D 1557 or not less than 80 percent of the relative density as determined by ASTM D 4253/ 4254 for free draining fill materials.

6.4 GROUNDWATER CONTROL

Groundwater may be encountered during construction excavation. The contractor should be prepared to perform dewatering or other appropriate groundwater control measures upon free water encountered during construction.

6.5 EXCAVATION SLOPES

Temporary excavations above the groundwater level should have side slopes not steeper than 1.5H:1V. Pertinent OSHA and local regulations should be followed where they require flatter side slopes than given above. Sheeting and shoring for excavations, if required, should be designed by an engineer registered in the Commonwealth of Pennsylvania.

6.6 CORROSION POTENTIAL

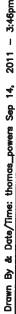
Corrosivity of steel should be evaluated by the structural and utility designers.

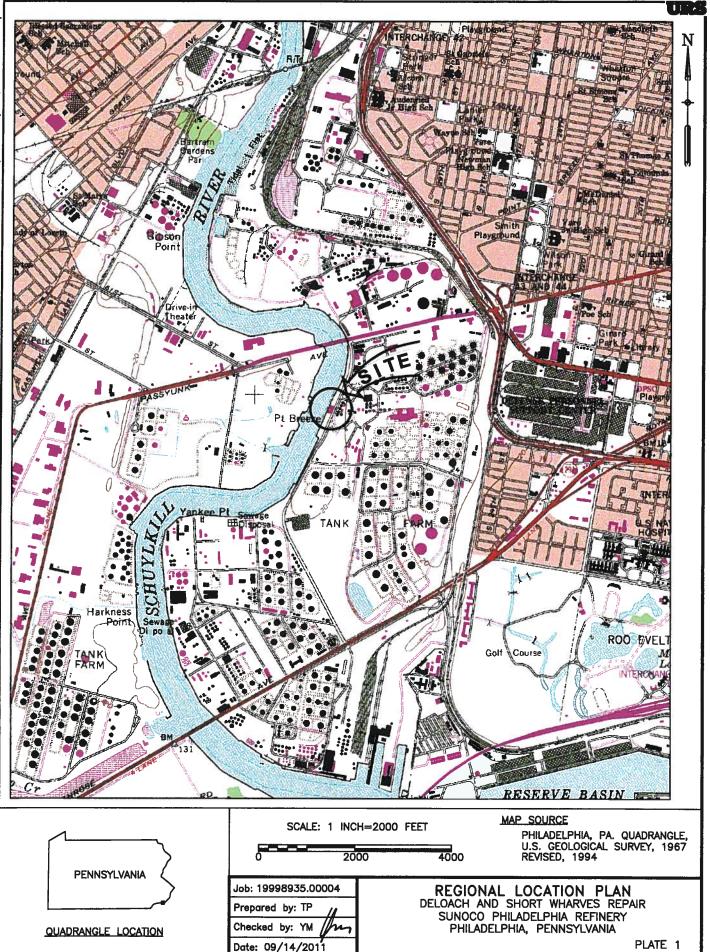
6.7 CONSTRUCTION OBSERVATION

It is recommended that full-time construction observation be provided during foundation and earthworks construction by URS Corporation or a qualified geotechnical engineering firm that is familiar with the subsurface conditions and the foundation design criteria. The items which should be observed, monitored, and/or tested include subgrade preparation, placement and compaction of structural fill, and pile construction.

The services described in this report were provided in accordance with reasonable and accepted engineering practice. No warranty or guarantee, expressed or implied, is intended. The conclusions and recommendations are based on the assumptions that the subsurface conditions do not deviate appreciably from those encountered in the test borings and pits and that the loads are similar to these given in the project description. If the structure is moved or loads have changed, URS should be given the opportunity to modify recommendations accordingly. The conclusions and recommendations are also based on competent field engineering, monitoring, and testing during construction. The recommendations presented in this report are solely for the use of our client for the design of this particular project. Any re-use of this document, particularly by third parties, without the express written permission of URS is solely at their own risk.

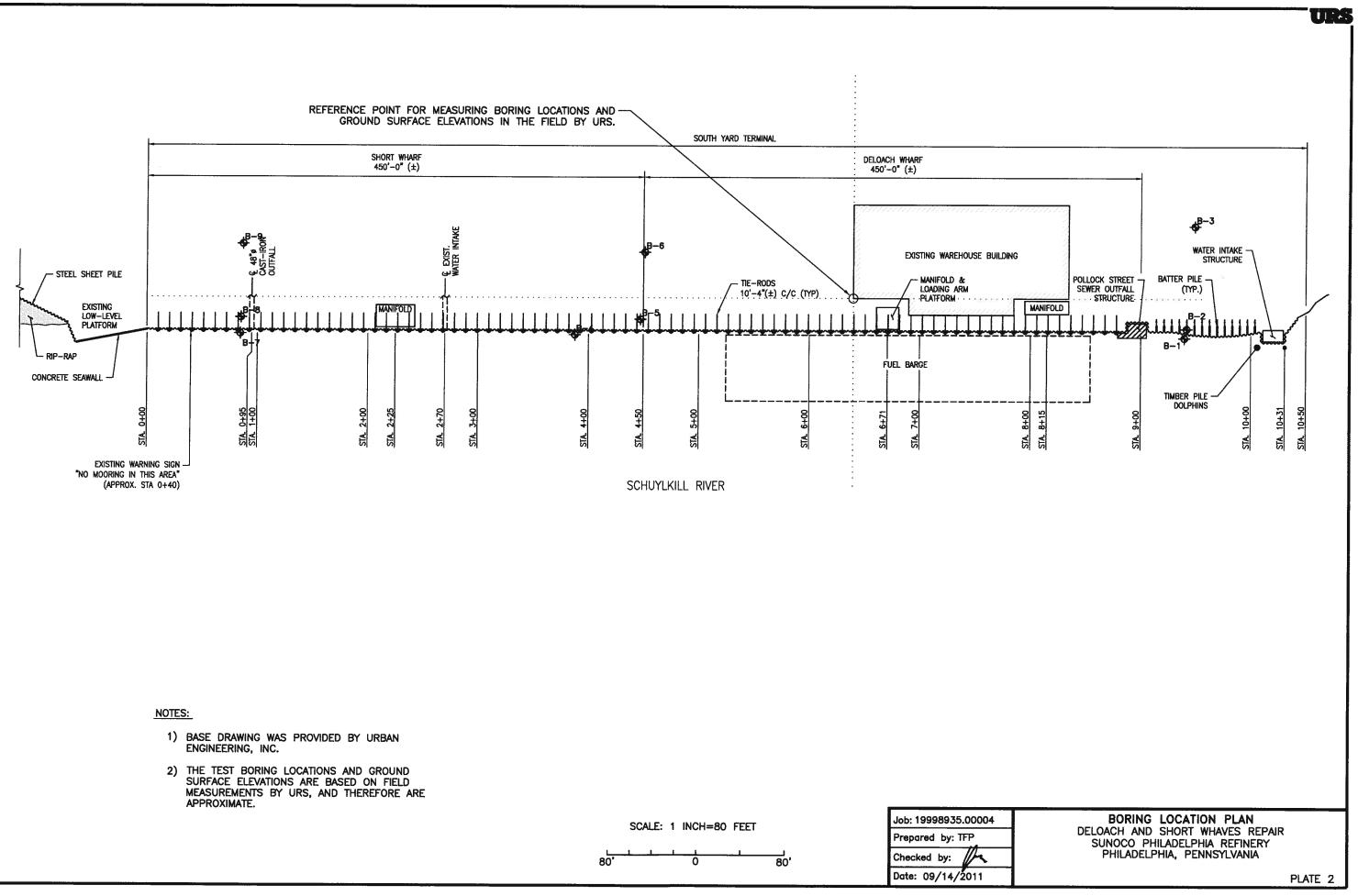
Plates

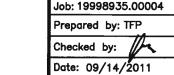


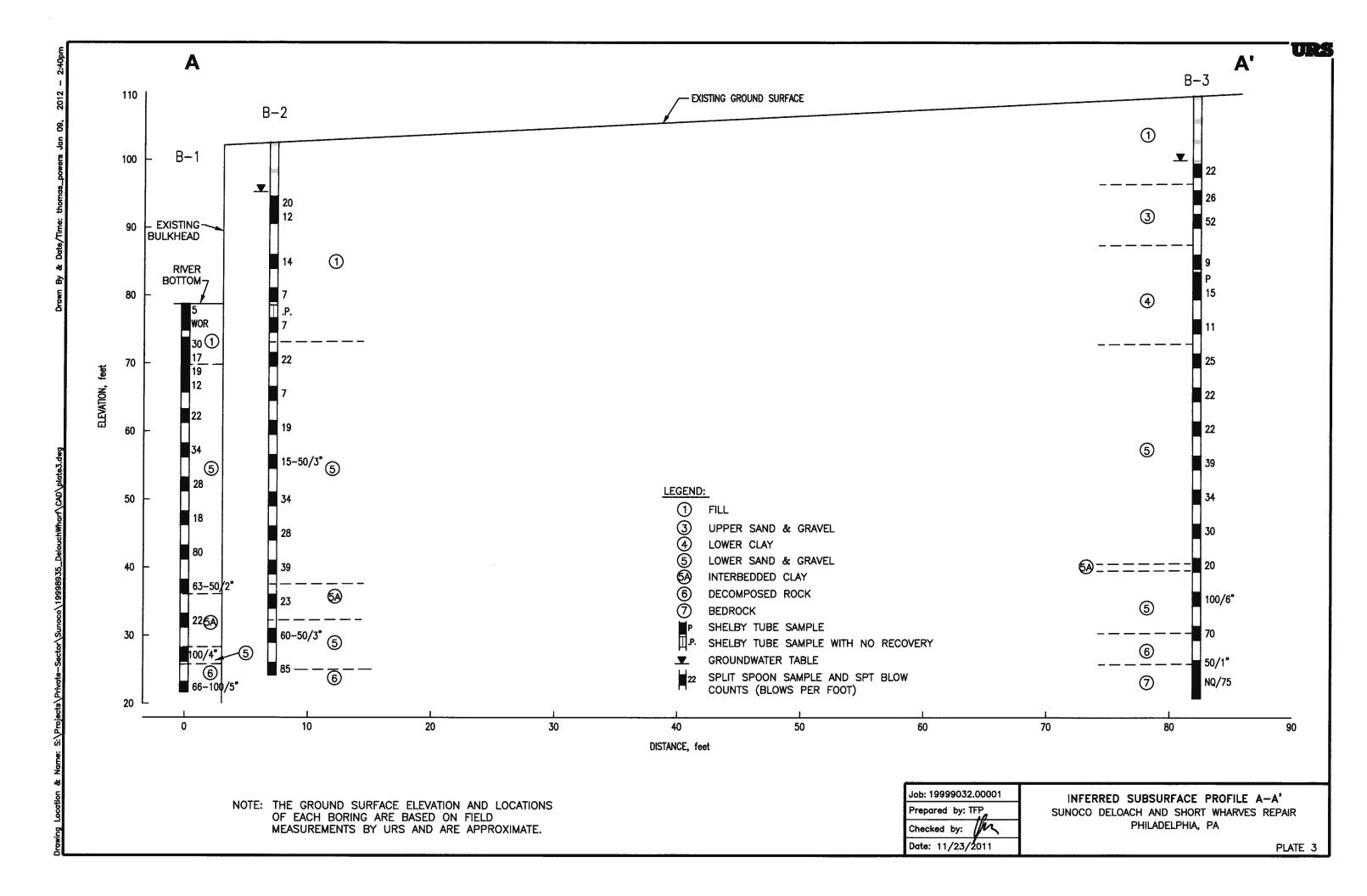


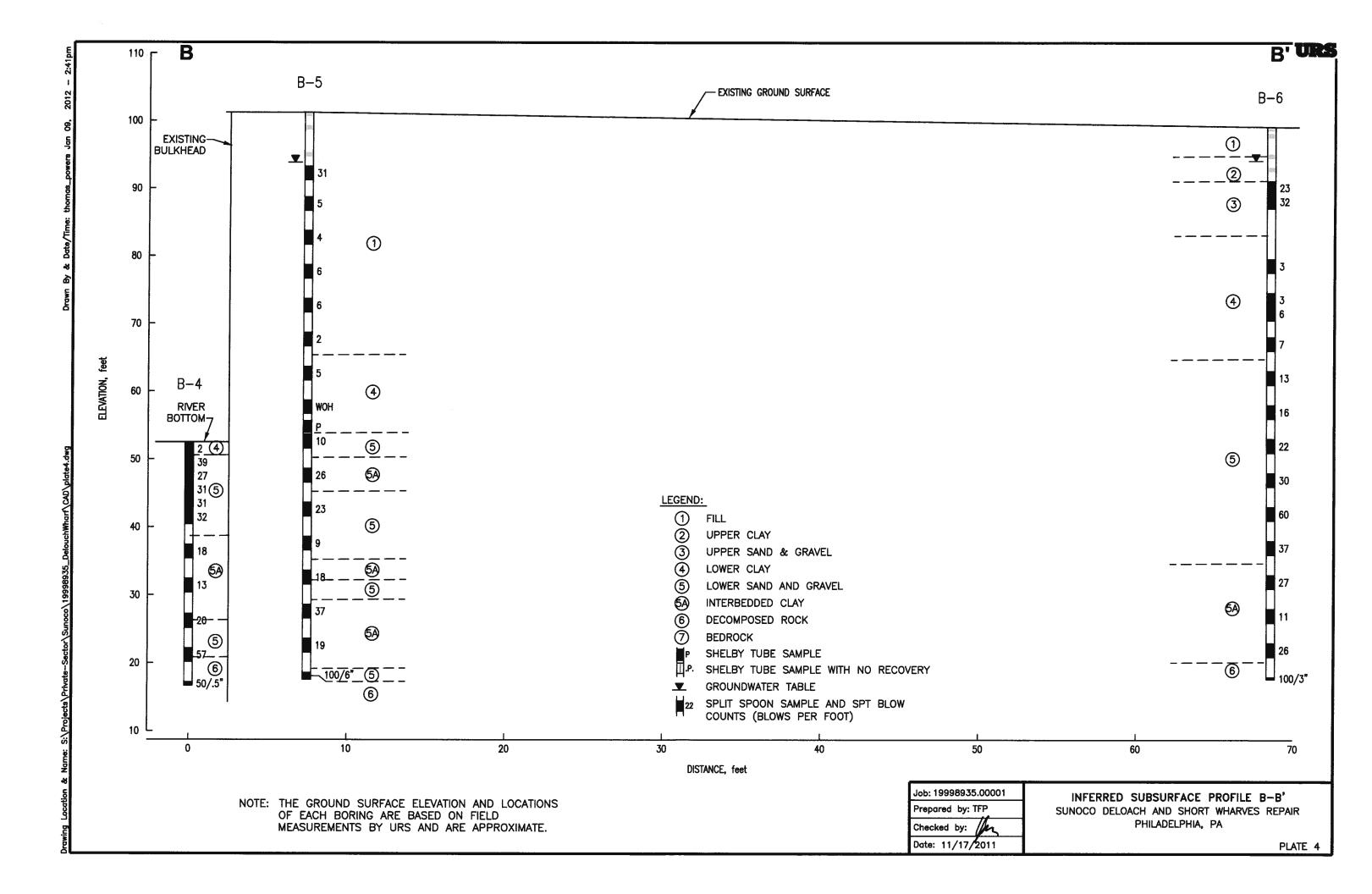
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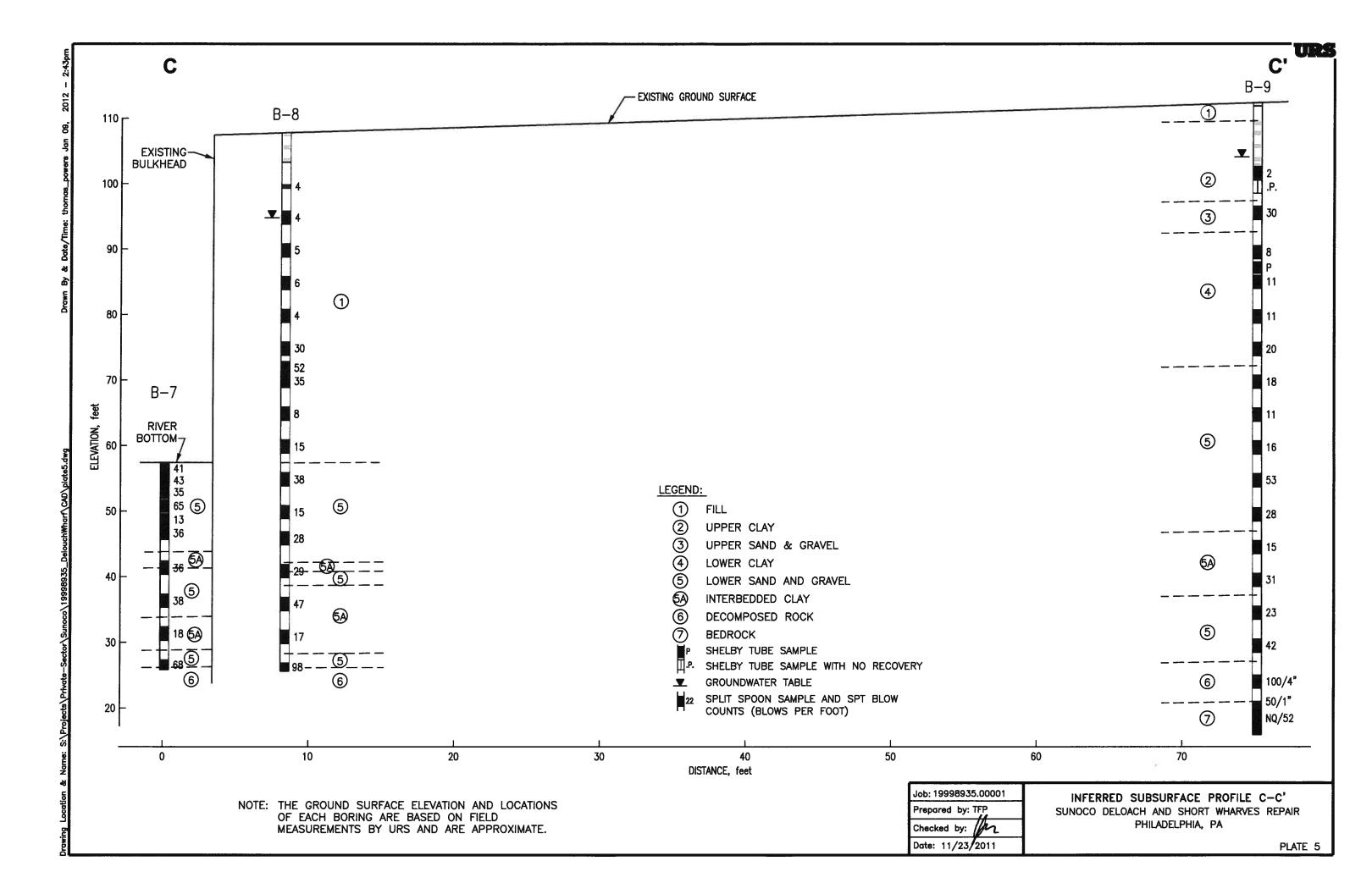
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Appendix A Subsurface Exploration The subsurface exploration consisted of nine test borings located as shown on Plate 2, Site and Boring Location Plan. The borings were drilled between July 19 and August 26, 2011, by Parratt-Wolff Inc., East Syracuse, New York. The test borings were conducted under full-time technical supervision of URS. The test borings were located in the field by URS with assistance from Sunoco personnel. Utility clearance was conducted by Sunoco using vacuum extraction techniques (hydro-excavation) at the top 10 feet of each boring on land. Test borings locations and elevations were interpreted based on field measurements by URS and are therefore approximate. The northwest corner of the existing maintenance warehouse was taken as El. +100 feet.

The soil conditions at the top ten feet of each land boring were evaluated through probing using a hand probe. Soil samples were obtained with a hand auger at various depths.

The test borings were performed using a truck-mounted CME 75 drilling rig and were advanced by mud-rotary drilling techniques and 4 inch OD casings. Samples of the subsoils were obtained from the borings for identification and classification purposes by means of a 2-inch O.D. splitbarrel sampler driven 24 inches by a 140-pound hammer freely falling 30 inches (the Standard Penetration Test, ASTM D 1586). The number of hammer blows required driving the sampler during the interval from 6 to 18 inches, or fraction thereof, is reported on the test boring logs as the sampling resistance. Relatively undisturbed samples of fine-grained soils were recovered using a 3-inch O.D. thin-walled Osterberg tube sampler in general accordance with ASTM D 1587.

NQ-size rock cores (1-7/8-inch diameter), approximately 5 feet in total length were obtained in two borings upon encountering bedrock. After coring, the Rock Quality Designation (RQD) was determined as the total length of all naturally segmented recovered rock core segments equal to or greater than 4 inches in length divided by the total length of each core run, expressed as a percentage. The RQD and the percent core recovery are presented on the boring logs.

Organic vapor monitoring was conducted during hydro-excavation and drilling operation by URS using a MiniRAE PID five gas monitor. The values of concentrations of organic vapor (in ppm) are shown on the boring logs under "Other Tests".

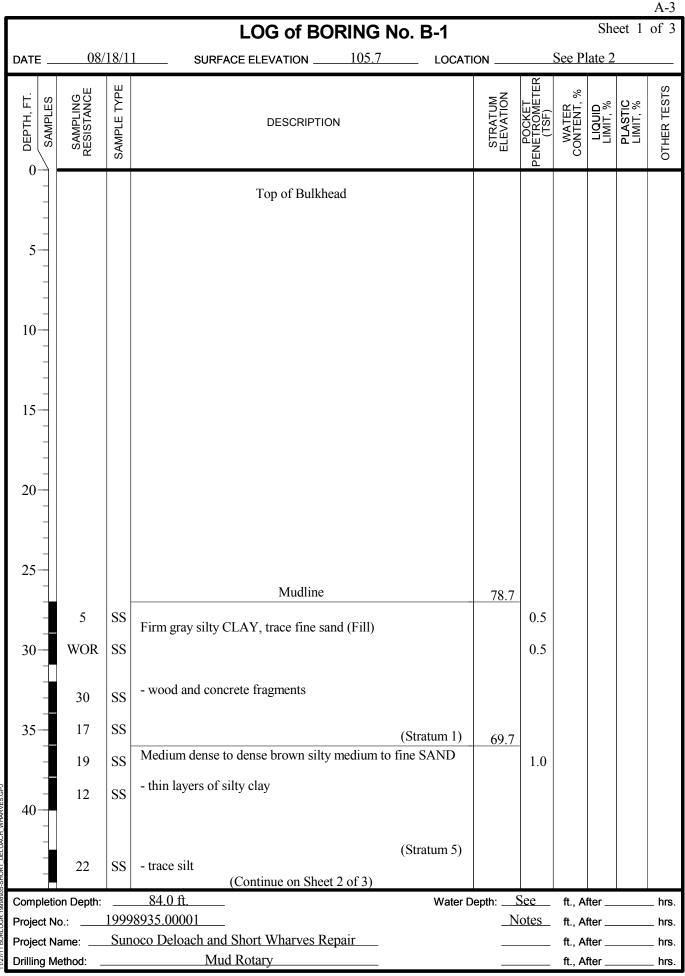
Where fine-grained materials were encountered, Pocket Penetrometer Resistance (PPR) readings were taken to obtain an indication of the unconfined compressive strength of cohesive soils. These values are shown on the boring logs under "Pocket Penetrometer (tsf)".

At the completion of the test borings, the boreholes were backed-filled with bentonite/cement grout.

A "Key to Soil Symbols and Terms" used in this report is included on page A-2. The logs of the test borings are presented on Pages A-3 through A-29.

KEY TO SOIL SYMBOLS AND TERMS	Terms used in this report for describing soils according to their texture or grain size distribution are in accordance with the Unified Soil Classification System, as described in Technical Memorandum No. 3-357, Waterways Experiment Station, March 1953.	TERMS DESCRIBING CONSISTENCY OR CONDITION	Description of the point in relatinge on No. 200 steps): Includes (1) clean gravels and (2) silly or licitaye gravels and sands. Condition is rated according to relative density(1) as determined by laboratory tests or standard penetration resistance tests. Descriptive Term Relative Density		Dense 65 to 85% Very dense 85 to 100%	FINE GRAINED SOILS (major portion passing No. 200 sieve): Includes (1) inorganic and organic sitis and clays, (2) gravelly, sandy, or sitity clays, and (3) clayey sits. Consistency is rated according to shearing strength, as indicated by penetrometer readings or by unconfined compression tests.	Descriptive Term Unconfined Compression Descriptive Term Strength, tons/sq, ft. Very soft less than 0.25	Soft 0.25 to 0.50 Firm 0.50 to 1.00 Stiff 1.00 to 2.00	Very stiff 2.00 to 4.00 Hard 4.00 and higher		P/250 P/250 Thin-wall tube pushed hydraulically, using a certain pressure (250 psi) to push the last 6 inches. Ci-Denison or Pitcher-Type - core-barrel sample. P		VS 20% – Rock Quality Designation (RQD) ⁽²⁾ VS - Vane Shear Test. Sample C – Consolitation and peoprite gravity tests. Recovered D – Maximum & minimum density.	e A C D N	Not T - Trioxial compression test. Recovered U - Unormitiend compression test. W - Unit weight & natural moisture content. X - Special tests performed – see Laboratory test results.	(2)ROD =∑Core Segments ≥ 4 Inches x 100 (1)ASTM 2049-69 Core Interval One Interval Where Segmentation is Not Caused By Drilling Effects
	01# 0	<pre>< ************************************</pre>		00	470.0 0.07470.0 0.20724.0 7.40700.3	D D		νW		#4 To 3/4 In. 3/4 In To 3 In. 3 In. To 12 In. 3 In. To 12 In. 11 30 To 36 In.		0 19.1 0 304.4 0 304.4	4.76Te		Fine Coarse Boulders	3
	əzig	2 evei2	əziS əlc	Partic	աա	1		Nater		eveiS	ezi2 eloit		uw		Material Gravel	
Laboratory classification criteria	= $\frac{D_{60}}{D_{10}}$ greater than 4: C_c = $\frac{(D_{20})^2}{D_{10}XD_{60}}$ between 1 and 3	Not meeting all gradation requirements for GW	Atterberg limits below "A" line or P.I. less than 4 Above "A" line with P.I.	between 4 and 7 are bor- Atterberg limits above "A" define cases requiring use of line-with P.I. greater than 7 duel symbols	$= \frac{D_{60}}{D_{10}}$ greater than 6; C _c = $\frac{(D_{30})^2}{D_{10} \times D_{60}}$ between 1 and 3	Not meeting all gradation requirements for SW	Atterberg limits below "A" line or P.I. less than 4 Limits plotting in hatched	Atterberg limits above "A" and 7 are bordenine cases line with P.I. $>$ than 7 requiring use of dual sym- bols.		5		HW Plue HO		CLE-MILLW ML and OL 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Liquid limit Plasticity Chart	*Division of GM and SM groups into subdivisions of d and u are for roads and airfields only. Subdivision is based on Atterberg limits; fix d used when L.L. is 28 or less and the P.L. is 6 or less; the suffix u used when L.L. is greater than 28. **Borderline classifications, used for soils possessing characteristics of two groups, are designated by combinations of group symbols.
-	ຶ			Bordetline o GM, GP, SM Bordetline o	ື	nt	than 5 per ce than 12 per 2 per cent.	Less ti More fot d	09	50		20 30	10			and airfields (when L.L. roups, are des
			əvəis 002 .o	o grain-size c N nert than N	ne noitserf)	senit to ege: swollo:	tneoreq no g d se beitisse	Dependini Dependini			xəbni y	Plasticity		Т	1	for roads ix u used of two gi
Typical names	Well-graded gravels, gravel-sand mix- ture, little or no fines	Poorly graded gravels, gravel-sand mixtures, little or no fines	Silty gravels, gravel-sand-silt mixtures	Clayey gravels, gravel-sand-clay mix- tures	Well-graded sands, gravelly sands, little or no fines	Poorly graded sands, gravelly sands, little or no fines	Silty sands, sand-silt mixtures	Clayey sands, sand-clay mixtures	Inorganic silts and very fine sands, rock flour, silty or clayey fine sands or clayey silts with slight plasticity	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, slity clays, lean clays	Organic silts and organic silty clays of low plasticity	Inorganic sitts, micaceous or diato- maceous fine sandy or sitty solls, elastic sitts	Inorganic clays of high plasticity, fat clays	Organic clays of medium to high plasticity, organic silts	Peat and other highly organic soils	*Division of GM and SM groups into subdivisions of d and u are for roads and airfields only. Subdivision is suffix d used when L.L. is 28 or less and the P.I. is 6 or less; the suffix u used when L.L. is greater than 28. *Borderline classifications, used for soils possessing characteristics of two groups, are designated by combina expertence.
Group symbols	GW	GP	۳ W3	ec	SW	SP	ws SM*	sc	ML	CL	OL	НМ	Н	Ю	ŧ	and SM g L. is 28 ifications,
Major Divisions	slavels	vels coarse fract á sieve siz	Gra fo half of ger than No sanif th finount fes)	stioc bania arger than N. Iarr Iarr Welsver Welsver Ideioard Ideio	noit: (92 sbns		Sar Safier thait of A nant thait Sanit th Sanit th Sanuome San San	MoroM) si si w sbn62 geiserqqA) if fo	(08 nsr	, 200 sieve) Silts and clays d limit less th	:		yelo bne stli		yinghiy organic slios	*Division of GM s suffix d used when L **Borderline class

A-2





				LOG of BORING No. B-1				Sh	eet 2	A-4 of 3
DATE		08/1	18/11		ON		See Pl	late 2		
DEPTH, FT.	SAMPLES	SAMPLING RESISTANCE	SAMPLE TYPE	DESCRIPTION	STRATUM ELEVATION	POCKET PENETROMETER (TSF)	WATER CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	OTHER TESTS
+5 		34	SS	Medium dense to dense brown coarse to fine SAND with varying amounts of gravel, trace silt						
55-	-	28	SS							
60-	-	18	SS	- thin layers of silty clay						
65-		80	SS	- sand and gravel						
70-		63- 0/2"	SS	(Stratum 5) Stiff to very stiff gray CLAY with thin partings of fine sand	36.2	-				
75-	-	22	SS	(Stratum 5A)	20.2	1.5- 2.0				
80-		00/4"	SS	- very dense gravel (Stratum 5A) (Stratum 5A) Very dense micaceous coarse to fine SAND and gravel-sized rock fragments (Decomposed Rock)	28.2	-				
85-		66- 00/5"	SS	(Stratum 6)	21.7	-				
-	-			(Continue on Sheet 3 of 3)						
Compl				<u>84.0 ft.</u> Water D	epth:					
Project Project				bco Deloach and Short Wharves Repair	_ <u>_1N</u>	otes				
Drilling			~	Mud Rotary						

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			LOG of BORING No. B-1					She	eet 3	of 3
DATE	08/	/18/11			J					
						ER				S
06 DEPTH, FT.	SAMPLING RESISTANCE	SAMPLE TYPE	DESCRIPTION		STRATUM ELEVATION	POCKET PENETROMETI (TSF)	WATER CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	OTHER TESTS
95-			Notes: 1. The drilling began at approximately 27 ft below the top of the bulkhead. All depths indicated in this log are from the top of the bulkhead. 2. Unless otherwise indicated, numerical values under "Other Tests" are PID readings from head space of sample jars (in ppm).							
115— - - - 120—										
125-										
130										
Completi	n Danth:			ter Dept	th: (See	£ ^	ftor		hro
Completic Project N			<u>8935.00001</u> Wa	ter Depi		lotes				
			boot Deloach and Short Wharves Repair							
			Mud Rotary							



A-5

								Sh	eet 1	A-6
DATE		08/	16/1	LOG of BORING No. B-2 1 SURFACE ELEVATION	-10N		See P			01 5
				$\frac{1}{1}$ SURFACE ELEVATION <u>104.5</u> LOCAT		ER			, 	
DEPTH, FT.	SAMPLES	SAMPLING RESISTANCE	SAMPLE TYPE	DESCRIPTION	STRATUM ELEVATION	POCKET PENETROMETE (TSF)	WATER CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	OTHER TESTS
0-			AU	Dense brown silty coarse to fine SAND and GRAVEL (Fill)						14
5-			AU							
10-		20	SS	- trace wood chips						
15-	-	12	SS	- uace wood emps						
20-		14	SS	- trace wood chips, concrete fragments						
25-	-	7	SS	- firm to stiff brown silty clay/clayey silt, trace fine sand						
30-	_	.P. 7	.P. SS	- brown medium to fine sand, trace silt, wood chips						
30-	-			(Stratum 1)	73.	0				
35-	-	22	SS	Medium dense to dense brown coarse to fine SAND with varying amounts of gravel, trace silt						
40-	-	7	SS	- sandy silty clay						
40-	-	19	SS	(Stratum 5) (Continue on Sheet 2 of 3)		Soc.		A .		
Comp Projec		n Depth:	<u> </u>	<u>80.3 ft.</u> Water I 8935.00001	-	See Notes				
-				oco Deloach and Short Wharves Repair	_		-			
Drillinę	g Me	thod: _		Mud Rotary	_		. ft., A	fter _		_ hrs.



43 Medium dense to dense brown coarse to fine SAND with varying amounts of gravel, trace silt 50 15- 50/3" SS 55 34 SS 60 28 SS 60 28 SS 61 39 SS 62 39 SS 65 39 SS 65 Stiff to very stiff gray CLAY with thin partings of fine sand	POCKET PENETROMETER (TSF) WATER CONTENT %		LIMIT, %
45	🏻 🎽		LIMIT, %
 4.3 4.3 4.5 4.5 4.5 50 50/3" SS 50/3" SS - medium to fine sand with thin layers of silty clay 60 28 SS - medium to fine sand with thin layers of silty clay 60 28 SS - medium to fine sand with thin layers of silty clay 60 28 SS - SS 			
55 34 SS 60 28 SS 65 39 SS 65 39 SS 70 23 SS 70 23 SS Stiff to very stiff gray CLAY with thin partings of fine sand 37.5 70 60- SS 75 60- SS			
60 39 SS 65 39 SS 70 23 SS 70 23 SS Stiff to very stiff gray CLAY with thin partings of fine sand 37.5 70 60- SS Very dense gray coarse to fine SAND and GRAVEL 32.5			
65 (Stratum 5) 37.5 70 23 SS Stiff to very stiff gray CLAY with thin partings of fine sand 70 23 SS Stiff to very stiff gray CLAY with thin partings of fine sand 70 60 SS Very dense gray coarse to fine SAND and GRAVEL			
70- 23 SS (Stratum 5A) 32.5 75 60- SS Very dense gray coarse to fine SAND and GRAVEL			
75 60- SS	2.5- 3.0		
85 SS SS (Stratum 5) 25.0 Very dense micaceous coarse to fine SAND and 24.2 gravel-sized rock fragments (Decomposed Rock) (Stratum 6)			
85- (Continue on Sheet 3 of 3) Completion Depth: 80.3 ft. Set		After	
		After	
Project Name: Sunoco Deloach and Short Wharves Repair	,	After	

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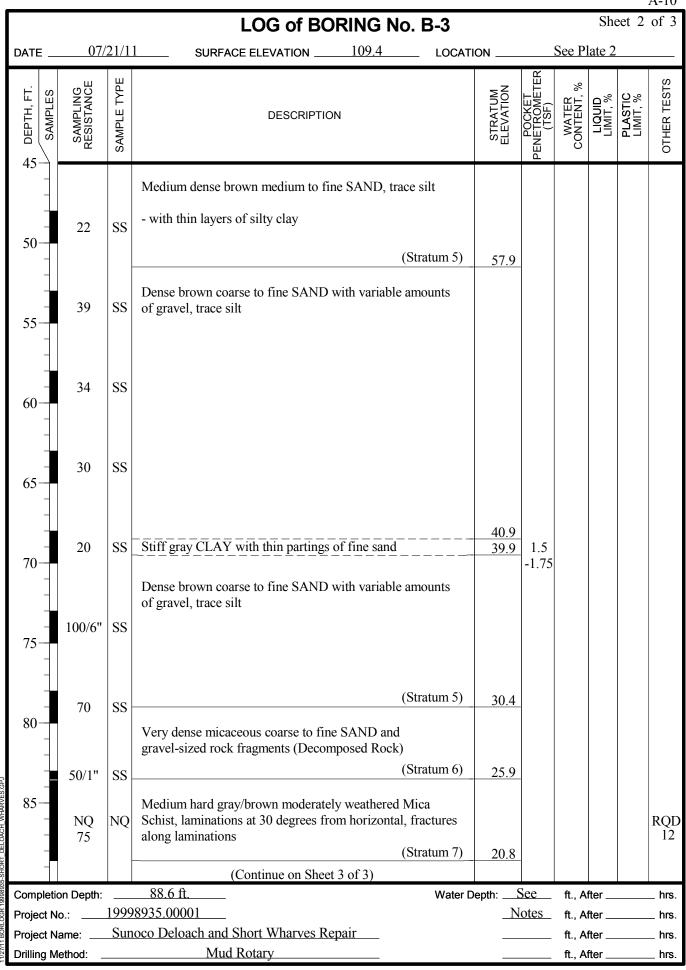
			LOG of BORING No. B-2				Sh	eet 3	A-8 of 3
DATE	08/1	6/11		ON		See P	late 2		
S DEPTH, FT. SAMPLES	SAMPLING RESISTANCE	SAMPLE TYPE	DESCRIPTION	STRATUM ELEVATION	POCKET PENETROMETER (TSF)	WATER, % CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	OTHER TESTS
90 95 100 105 110 110 115 120 125 130 Completio			Notes: 1. The boring was advanced to approximately 10 ft depth using vacuum excavation method (hydro-excavation). The soils resistance was evaluated using a hand probe. Samples were obtained using a hand auger at various depths. 2. Unless otherwise indicated, numerical values under "Other Tests" are PID readings from head space of sample jas (in ppm). 3. Groundwater was measured in the monitoring well. <u>Date GW Depth (ft) GW Elev (ft)</u> <u>8/26/2011 9.3 95.2</u>	enth.			fter		
Project No		9999	8935.00001	-	lotes				
Project Na			oco Deloach and Short Wharves Repair						
Drilling Me	ethod:		Mud Rotary			ft., A	fter		_ hrs.



			LOG of BORING No. B-3				She	eet 1	A-9
DATE	07/	/21/11		ON		See P	late 2		
DEPTH, FT.	SAMPLING RESISTANCE	SAMPLE TYPE	DESCRIPTION	STRATUM ELEVATION	POCKET PENETROMETER (TSF)	WATER CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	OTHER TESTS
		AU	Dense brown silty coarse to fine SAND and GRAVEL,						
5-		AU	brick and concrete fragments (Fill)						100
-		AU							29
		AU	- wood and brick fragments						40
-	22	SS	(Stratum 1)	96.4					
15-	26	SS	Medium dense brown medium to fine SAND, trace silt		-				
	52	SS	- becoming very dense brown coarse to fine sand and gravel						
			(Stratum 3)	87.4					
-	9	SS	Stiff gray fine sandy silty CLAY		1.25-				
25-	D				1.5	26.2	12	25	
	Р 15	P SS	- becoming fine sandy silt		1.5- 1.75	26.3	42	25	M
_									
35-	11	SS							
- - 40	25	SS	(Stratum 4) Medium dense brown medium to fine SAND, trace silt	72.9	-				
	22	SS	(Stratum 5)						
Completion			(Continue on Sheet 2 of 3) <u>88.6 ft.</u> Water D	epth:	See	ft., A	fter		h
Project No	.:	1999	8935.00001	-	otes	ft., A	fter		h
Project Na		Suno	be Deloach and Short Wharves Repair				fter		
Drilling Me	thod: _		Mud Rotary TTDC			ft., A	fter		h

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<u>A-</u>9



A-10

		1 SURFACE ELEVATION									
NG			109.4			See Plate 2					
SAMPLING RESISTANCE	SAMPLE TYPE	DESCRIPTIO	N		STRATUM ELEVATION	PENETROMETER (TSF)	WATER CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	OTHER TESTS	
		using vacuum excavation method (h soils resistance was evaluated using were obtained using a hand auger at 2. Unless otherwise indicated, nume "Other Tests" are PID readings from jars (in ppm). 3. Groundwater was measured in the	ydro-excavatio a hand probe. various deptha rical values ur head space of e monitoring w	on). The Samples s. nder f sample							
-		<u> 88.6 ft. </u> 28935 00001		Water D	-						
	on Depth: o.: ame:	ame: <u>Sur</u>	1. The boring was advanced to approusing vacuum excavation method (h soils resistance was evaluated using were obtained using a hand auger at 2. Unless otherwise indicated, nume "Other Tests" are PID readings from jars (in ppm). 3. Groundwater was measured in the Date GW Depth (ff) 98/12/2011 11.5 8/12/2011 11.5 8/23/2011 9.6 8/26/2011 10.0	1. The boring was advanced to approximately 10 f using vacuum excavation method (hydro-excavatios soils resistance was evaluated using a hand probe. were obtained using a hand auger at various depth 2. Unless otherwise indicated, numerical values un "Other Tests" are PID readings from head space or jars (in ppm). 3. Groundwater was measured in the monitoring w Date GW Depth (ft) GW Elev (ft) 8/12/2011 11.5 97.9 8/18/2011 11.5 97.9 8/26/2011 9.6 99.8 8/26/2011 10.0 99.4	I. The boring was advanced to approximately 10 ft depth using vacuum excavation method (hydro-excavation). The soils resistance was evaluated using a hand probe. Samples were obtained using a hand auger at various depths. I. Unless otherwise indicated, numerical values under "Other Tests" are PID readings from head space of sample jars (in ppm). 3. Groundwater was measured in the monitoring well. Date GW Depth (ft) GW Elev (ft) 8/12/2011 11.7 97.7 8/18/2011 11.5 97.9 8/23/2011 9.6 99.8 8/26/2011 10.0 99.4	I. The boring was advanced to approximately 10 ft depth using vacuum excavation method (hydro-excavation). The soils resistance was evaluated using a hand auger at various depths. I. Unless otherwise indicated, numerical values under "Other Tests" are PID readings from head space of sample jars (in ppm). 3. Groundwater was measured in the monitoring well. Date <u>GW Depth (ft)</u> 8/12/2011 11.7 97.9 8/23/2011 9.6 99.8 8/26/2011 10.0 99.4	I. The boring was advanced to approximately 10 ft depth using vacuum excavation method (hydro-excavation). The soils resistance was evaluated using a hand arger at various depths. 2. Unless otherwise indicated, numerical values under "Other Tests" are PID readings from head space of sample jars (in ppm). 3. Groundwater was measured in the monitoring well. Date GW Depth (ft) 8/12/2011 11.7 97.7 8/18/2011 11.5 97.8 8/23/2011 9.6 99.8 8/26/2011 10.0 99.4	I. The boring was advanced to approximately 10 ft depth using vacuum excavation method (hydro-excavation). The soils resistance was evaluated using a hand probe. Samples were obtained using a hand auger at various depths. 2. Unless otherwise indicated, numerical values under "Other Tests" are PID readings from head space of sample jars (in ppm). 3. Groundwater was measured in the monitoring well. Date GW Depth (ft) 6 GW Depth (ft) GW Elev (ft) 8/18/2011 11.7 97.7 8/18/2011 11.5 97.9 8/26/2011 10.0 99.4 State of the source of sample jars (in ppm). 3. Groundwater was measured in the monitoring well. 8/26/2011 10.0 99.4 state of the source of sample source of source	I. The boring was advanced to approximately 10 ft depth using vacuum excavation method (hydro-excavation). The soils resistance was evaluated using a hand probe. Samples were obtained using a hand auger at various depths. I. Unless otherwise indicated, numerical values under "Other Tests" are PID readings from head space of sample jars (in ppm). 3. Groundwater was measured in the monitoring well. Date <u>GW Depth (ft)</u> Stars (in ppm). 3. Groundwater was measured in the monitoring well. Date <u>GW Depth (ft)</u> Stars (in ppm). 3. Groundwater was measured in the monitoring well. 912 (Stars) 923 (2011) 10.0 99.4	n. The boring was advanced to approximately 10 ft depth using vacuum excavation method (hydro-excavation). The soils resistance was evaluated using a hand auger at various depths. 2. Unless otherwise indicated, numerical values under "Other Tests" are PID readings from head space of sample jars (in ppm). 3. Groundwater was measured in the monitoring well. Date GW Depth (ft) GW Elev (ft) \$/12.2011 11.5 97.9 8/23.2011 9.6 99.8 8/26/2011 10.0 99.4 %18/2011 11.5 97.9 8/23.2011 9.6 99.8 8/26/2011 10.0 99.4 %20/2011 10.0 99.4 %20/20011 10.0 99.4 %20/20011 10.0 99.4 %20/20011 10.0 99.4 %20/20011 10.0 99.4	



			LOG of BOR	NG No. E	3-4				She		of 3
DATE	07/2	29/1				ON		See Pl	late 2		
0 DEPTH, FT.	SAMPLING RESISTANCE	SAMPLE TYPE	DESCRIPTION			STRATUM ELEVATION	POCKET PENETROMETER (TSF)	WATER CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	OTHER TESTS
			Top of Bulkhead								
-			ľ								
5											
15-											
20-											
25-											
30											
35-											
40											
_			(Continue on Sheet 2 c	of 3)							
Completio			87.2 ft.		Water D						
Project No			<u>8935.00001</u>			<u>_N</u>	lotes				
			oco Deloach and Short Wharves Repai Mud Rotary	<u>r</u>							_ hrs. _ hrs.
ווווחס Me	=u100: _		IVIUU INDIALY					π., A	iter		_ nrs.



A-12

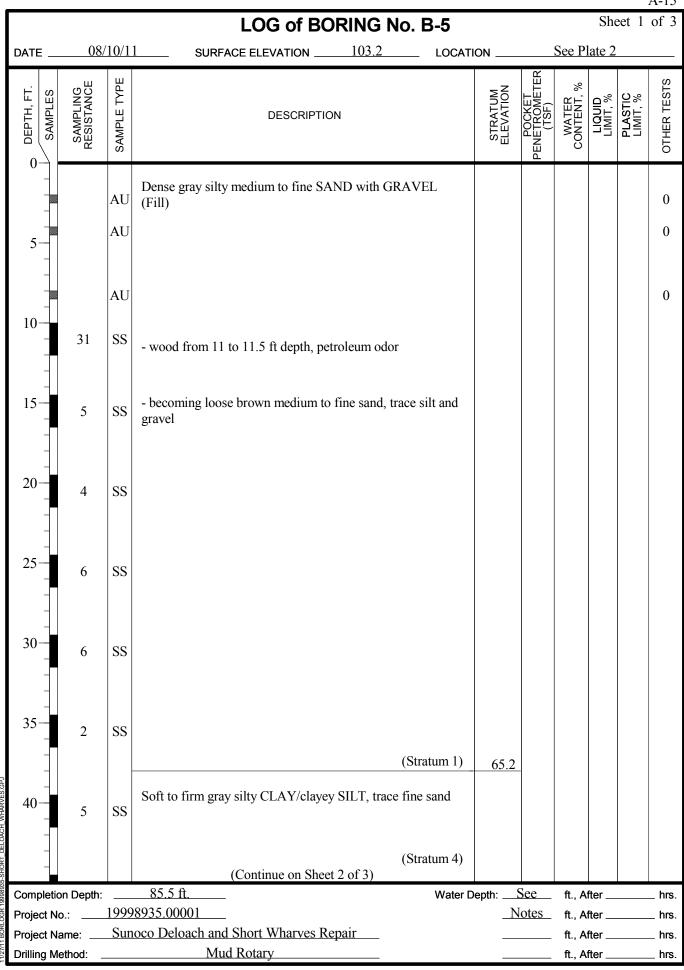
LOG of BORING No. B-4 Sheet 2 of								A-13 of 3	
DATE									-
APTH, FT.	SAMPLING RESISTANCE	SAMPLE TYPE	DESCRIPTION	STRATUM ELEVATION	POCKET PENETROMETER (TSF)	%	LIQUID LIMIT, %	PLASTIC LIMIT, %	OTHER TESTS
- - - 50- - -	2	SS	Mudline Very soft to soft brown silty CLAY, trace organic (Stratum 4)	<u>52.5</u> 50.5	0.5				
55 - - -	39 27 31	SS SS SS	Stiff to very stiff brown silty CLAY, trace fine sand Medium dense to dense gray coarse to fine SAND with varying amounts of gravel, trace silt	49.5	-				
- 60 - -	31	SS SS							
65- - - - 70-	18	SS	(Stratum 5) Stiff to very stiff dark gray CLAY with thin partings of fine sand	39.0	1.5				
	13	SS			1.5- 2.0				
- - - 80 -	20	SS	(Stratum 5A) Medium dense to very dense gray coarse to fine SAND and GRAVEL, trace silt, occasional thin layers of silty clay	26.3	0.5-1.0				
- - 85	57	SS	(Stratum 5) Very dense micaceous coarse to fine sand and gravel-sized rock fragments (Decomposed Rock)	20.8					
85 - - -	50/.5"	SS	(Stratum 6) (Continue on Sheet 3 of 3) 87.2 ft. Water D	16.8	Sec	£	har		h
Completi Project N	on Depth:	1999	<u>8/.2 п.</u> Water D 8935.00001	epth: <u> </u>	otes				
-	,		Sunoco Deloach and Short Wharves Repair			ft., After			
Drilling N	lethod: _		Mud Rotary			ft., Af	ter		_ hrs.



	A-14 LOG of BORING No. B-4 Sheet 3 of 3								
DATE	07	/29/11		TION		See P			01 5
06 DEPTH, FT.	SAMPLING RESISTANCE	SAMPLE TYPE	DESCRIPTION	STRATUM FI FVATION	POCKET PENETROMETER (TSF)	WATER CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	OTHER TESTS
95- - - - - - - - - - - - - - - - - - -			 Notes: 1. The drilling began at approximately 51.5 ft below the top of the bulkhead. All depths indicated in this log are from the top of the bulkhead. 2. Drilling resistance (i.e., rig chatter) was encountered at approximately 83 ft depth. 3. Unless otherwise indicated, numerical values under "Other Tests" are PID readings from head space of sample jars (in ppm). 						
120									
- 130 - - - -									
Completio			<u>87.2 ft.</u> Water 8935.00001	r Depth: _					
Project No Project Na			bco Deloach and Short Wharves Repair	-	Notes				
Drilling M		~ 411	Mud Rotary	-			fter		_ nrs. _ hrs.



<u>A-</u>14



							Sh	eet 2	A-16
	0.0/	10/1	LOG of BORING No. B-5			Cao Di			01 5
DATE	08/	10/1	1 SURFACE ELEVATION 103.2 LOCATI	ON		See Pl	late 2		
5 DEPTH, FT.	SAMPLING RESISTANCE	SAMPLE TYPE	DESCRIPTION	STRATUM ELEVATION	POCKET PENETROMETEF (TSF)	WATER CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	OTHER TESTS
43	WOH	SS	Soft to firm gray silty CLAY, trace fine sand						
-	Р	Р	(Stratum 4)	53.7	0.5	32.8	30	22	МΤ
50— - -	10	SS	Medium dense brown silty coarse to fine SAND, with thin layers of silty clay (Stratum 5)	50.2	-				
- 55 - -	26	SS	Very stiff dark brown CLAY, trace fine sand (Stratum 5A)	45.2	2.5- 3.0				
- 60 -	23	S3	Medium dense brown coarse to fine SAND and GRAVEL, trace silt with thin layers of silty clay						
65— - -	9	SS	- becoming loose medium to fine sand (Stratum 5)	35.2					
- 70 - -	18	SS	Stiff to very stiff dark gray CLAY, trace fine sand (Stratum 5A) Medium dense dark gray medium to fine SAND, trace silt (Stratum 5)	<u>32.2</u> 30.2	1.5-				
75	37	SS	Stiff to very stiff gray CLAY, trace fine sand with thin partings of fine sand, and occasional thin layers of coarse to fine sand		1.5				
80	19	SS			1.75- 2.5				
85-	100/6"	SS	(Stratum 5A) Very dense gray coarse to fine SAND and GRAVEL, trace silt (Stratum 5) Very dense micaceous coarse to fine SAND and gravel-sized rock fragments (Decomposed Rock) (Stratum 6)	20.2 18.2 17.7					
Completi	on Depth:		85.5 ft Water D	epth:	See	ft., A	fter		_ hrs
Project N	-		8935.00001	•	otes				
-			oco Deloach and Short Wharves Repair						
Drilling M	ethod: _		Mud Rotary			ft., A	fter		_ hrs

				LOG of BORI	NG No.	B-5				Sh	eet 3	of .
DATE		08/	/10/11	SURFACE ELEVATION	103.2	_ LOCATI	ON		See P	late 2	,	
06 DEPTH, FT.	SAMPLES	SAMPLING RESISTANCE	SAMPLE TYPE	DESCRIPTION			STRATUM ELEVATION	POCKET PENETROMETER (TSF)	WATER CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	OTHER TESTS
				Notes: 1. The boring was advanced to approximusing vacuum excavation method (hydr soils resistance was evaluated using a h were obtained using a hand auger at van 2. Unless otherwise indicated, numerica "Other Tests" are PID readings from he jars (in ppm). 3. Groundwater was measured in the me <u>Date GW Depth (ft) GW</u> 8/23/2011 9.3 8/26/2011 9.6	o-excavation and probe. S ious depths al values und ad space of	n). The Samples der Sample						
- - 115— -												
120— - -	-											
130— - - -												
Comple	etior	n Depth:		85.5 ft.		Water D	epth:		ft., A	fter _		_ h
Project				8935.00001			_ <u>N</u>	otes	ft., A	fter _		_ h
Draiget	No	me:	Sun	oco Deloach and Short Wharves Repai	r				€ ∧	ftor		_ h



							Sheet 1	A-18
DATE	06	/27/1	LOG of BORING No. B-6 1	ON		See Plate		01 5
			SURFACE ELEVATION LOCATI	UN	ſĽ			
DEPTH, FT.	SAMPLING RESISTANCE	SAMPLE TYPE	DESCRIPTION	STRATUM ELEVATION	POCKET PENETROMETEI (TSF)	WATER CONTENT, % LIQUID	LIMIT, % PLASTIC LIMIT, %	OTHER TESTS
		AU AU	Dense brown silty coarse to fine SAND and GRAVEL (Fill)					300
5-		AU	(Stratum 1)	94.6				400
		AU	Firm to stiff dark gray sandy silty CLAY					800
10	23	SS	(Stratum 2)	91.1				
	32	SS	Medium dense to dense brown coarse to fine SAND and GRAVEL, trace silt					
15-			(Stratum 3)	02.1				
20-			Soft to firm gray silty CLAY/clayey SILT, trace fine sand	83.1				
-	3	SS			0.5			
25-								
	3	SS	- fine sandy silt		0.5			
30	6	SS	- fine sandy silt		0.5			
35-	7	SS	- clayey silt (Stratum 4)	64.6	0.5			
40 	13	SS	Medium dense brown medium to fine SAND, trace silt, occasional thin layers of silty clay					
	16	SS	(Stratum 5) (Continue on Sheet 2 of 3)					
Completio				epth:		ft., After		_ hrs.
Project N			<u>8935.00001</u>	<u>N</u>	otes	ft., After		
Project N		Sun	oco Deloach and Short Wharves Repair Mud Rotary			ft., After		
Drilling M						ft., After		_ hrs.

							Sh	eet 2	A-19
		77/1	LOG of BORING No. B-6						01 5
DATE	06/.	2//1	1 SURFACE ELEVATION 101.1 LOCATI	ON		See Pl	late 2		
. DEPTH, FT. SAMPLES	SAMPLING RESISTANCE	SAMPLE TYPE	DESCRIPTION	STRATUM ELEVATION	POCKET PENETROMETER (TSF)	WATER CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	OTHER TESTS
	22	SS	Medium dense brown medium to fine SAND, trace silt, occasional thin layers of silty clay						
55 - - - -	30	SS	(Stratum 5) - becoming dense to very dense gray coarse to fine sand with variable amounts of gravel, trace silt						
- - 60	60	SS							
65-	37	SS	- becoming medium to fine sand (Stratum 5)	34.6	-				
70	27	SS	Very stiff dark gray CLAY with thin partings of fine sand						
75	11	SS							
80-	26	SS	(Stratum 5A)	20.1	_				
85-	100/3"	SS	Very dense micaceous coarse to fine SAND and gravel-sized rock fragments (Decomposed Rock) (Stratum 6)/	17.8	-				
Completic	on Depth.		(Continue on Sheet 3 of 3) 	epth:	See	ft A	fter		hrs
Project N		1999	8935.00001	-	lotes				
-		Sun	oco Deloach and Short Wharves Repair						
Drilling M	ethod: _					ft., A	fter _		_ hrs.



<u>A-19</u>

	LOG of BORING No. B-6 Sheet 3							A-20	
						~ ~			01 5
DATE _	0	6/27/1	1 SURFACE ELEVATION101.1 LOCAT	TON	_	See P	late 2		
DEPTH, FT.	SAMPLING RESISTANCE	SAMPLE TYPE	DESCRIPTION	STRATUM ELEVATION	POCKET PENETROMETER (TSF)	WATER CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	OTHER TESTS
90 95 			Notes: 1. The boring was advanced to approximately 10 ft depth using vacuum excavation method (hydro-excavation). The soils resistance was evaluated using a hand probe. Samples were obtained using a hand auger at various depths. 2. No sampling between 14 ft and 21.5 ft due to high LEL readings. 3. Unless otherwise indicated, numerical values under "Other Tests" are PID readings from head space of sample jars (in PPM). 4. Groundwater was measured in the monitoring well. <u>Date GW Depth (ft) GW Elev (ft)</u> 8/23/2011 7.1 94.0						
Complet	tion Dept	ו:	83.3 ft. Water I	Depth:	See	ft A	fter _		_ hrs.
Project I			<u>8935.00001</u>	-	Notes				
			oco Deloach and Short Wharves Repair	_		,			
-			Mud Rotary	_					



			LOG of BORI	NG No. B-7				She		of 3
DATE	07/	27/1			ATION _		See P	late 2	,	
0 DEPTH, FT.	SAMPLING RESISTANCE	SAMPLE TYPE	DESCRIPTION		STRATUM	PENETROMETER	WATER CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	OTHER TESTS
			Top of Bulkhead							
-			·F · · · · · ·							
5										
10-										
15-										
20-										
25-										
30-										
35-										
40-										
			(Continue on Sheet 2 o	f 3)						
Completic		·	84.0 ft.		er Depth:	See	. ft., A	fter		_ hrs.
Project No			8935.00001			Notes	-			
Project Na			oco Deloach and Short Wharves Repair	·						
Drilling Me	ethod: _		Mud Rotary				. ft., A	fter		_ hrs.



			LOG of BORING No. B-7				She	et 2	A-22 of 3
DATE	07/	27/1		ON		See Pl			
DEPTH, FT. SAMPLES	SAMPLING RESISTANCE	SAMPLE TYPE	DESCRIPTION	STRATUM ELEVATION	POCKET PENETROMETER (TSF)	WATER CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	OTHER TESTS
	41 43 35 65 13 36	SS SS SS SS SS SS	Mudline Dense brown silty coarse to fine SAND and GRAVEL - becoming dense coarse to fine sand, trace silt, gravel - medium dense (Stratum 5) Very stiff dark gray CLAY with thin partings of fine sand (Stratum 5A)	<u>57.4</u> 43.8 41.3	1.75-	7.4 11.2 11.8 15.6 10.5 39.0	62	25	M M M M M
70- - - 75- - - - - - - - - - - - - - - -	38 18	SS	Dense gray coarse to fine SAND, trace silt, gravel - sand and gravel (Stratum 5) Stiff to very stiff gray clay with thin layers of fine sand (Stratum 5A) Very dense SAND and GRAVEL (Stratum 5A)	<u>33.8</u> 28.8	2.0	12.2 27.8	53	20	M M
85- - - - Completic Project N Project N Drilling M	o.: ame:		(Stratum 5) Very dense micaceous coarse to fine sand and gravel-sized rock fragments (Decomposed Rock) (Stratum 6) (Continue on Sheet 3 of 3) <u>84.0 ft.</u> <u>8935.00001</u> <u>oco Deloach and Short Wharves Repair</u> <u>Mud Rotary</u>	 	See	ft., A ft., A	fter fter		_ hrs. _ hrs.



<u>A-22</u>

	A-23								
	~ -		LOG of BORING No. B-7			~ ~			01 5
DATE	07/	/27/1	SURFACE ELEVATION109.8 LOCAT			See P	late 2	1	
06 DEPTH, FT.	SAMPLING RESISTANCE	SAMPLE TYPE	DESCRIPTION	STRATUM ELEVATION	POCKET PENETROMETER (TSF)	WATER CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	OTHER TESTS
95-			Notes:1. The drilling began at approximately 52.4 ft below the top of the bulkhead. All depths indicated in this log are from the top of the bulkhead.2. Loss of drilling fluid noted at approximatley 61 ft and 81 ft depths.						
- 100 - - -									
105									
110									
115									
120-									
125— — — — — —									
Completic				Depth:					
Project No			8935.00001		lotes				
Project Na		Sun	oco Deloach and Short Wharves Repair						
Unilling Me	Drilling Method: ft., After						_ hrs		



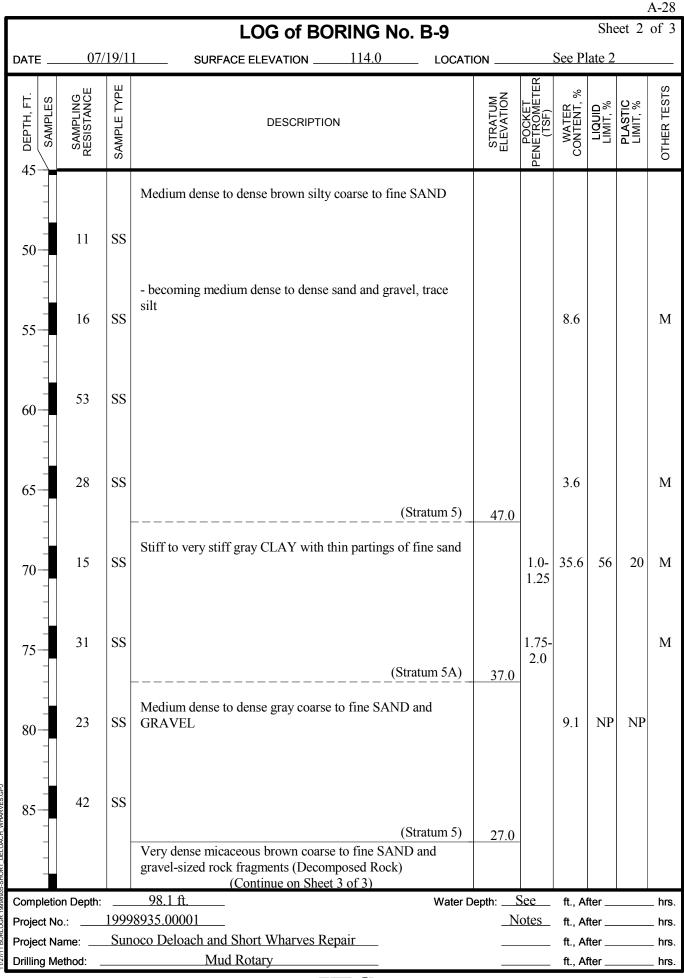
							Sh		A-24 of 3
	~ ~ ~	0-1-	LOG of BORING No. B-8			0 -			01.3
DATE	06/.	27/11	SURFACE ELEVATION109.8 LOCATI	ON		See P	late 2		
DEPTH, FT.	SAMPLING RESISTANCE	SAMPLE TYPE	DESCRIPTION	STRATUM ELEVATION	POCKET PENETROMETER (TSF)	WATER CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	OTHER TESTS
- - - - - - - - - -		AU AU AU	Dense brown silty coarse to fine SAND and GRAVEL (Fill) - brown silty coarse to fine sand - medium dense sand and gravel						1000 1000 3000
	4	SS	- becoming loose silty fine sand			20.8			М
- 15 - -	4	SS							
20	5	SS	- trace clay						
25-	6	SS				27.8			М
30-	4	SS							
35-	30	SS	- approximately 6" of wood						
-	52	SS	- concrete and brick fragments						
40	35	SS	- concrete and brick fragments (Stratum 1)			14.1			М
			(Stratum 1) (Continue on Sheet 2 of 3)						
Completio				epth:					
Project No			8935.00001	N	lotes				
Project Na Drilling Me		Sun	oco Deloach and Short Wharves Repair Mud Rotary						
						п., А			_ 115.

			LOG of BORING No. B-8				She	eet 2	of 3
DATE	06/	/27/11	SURFACE ELEVATION109.8 LOCATI	ON		See P	late 2		
DEPTH, FT. SAMPLES	SAMPLING RESISTANCE	SAMPLE TYPE	DESCRIPTION	STRATUM ELEVATION	POCKET PENETROMETER (TSF)	WATER CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	OTHER TESTS
45	8	SS	- brown sandy silt			32.7	37	25	Μ
50-	15	SS	- medium dense brown silty sand with concrete/brick fragments (Stratum 1)	57.3					
55-	38	SS	Medium dense to dense coarse to fine SAND with varying amounts of gravel, trace silt						
60-	15	SS				8.2			N
65-	28	SS							
70	29	SS	(Stratum 5) Stiff silty CLAY with fine sand (Stratum 5A) Medium dense dark gray silty coarse to fine SAND (Stratum 5)	42.3 40.8 38.8					
75	47	SS	Very stiff dark gray silty CLAY with thin partings of fine sand		1.0- 1.75	43.7	61	26	N
- - 80	17	SS	(Stratum 5A)	28.3	1.75- 2.0				
85-	98	SS	Very dense coarse to fine SAND and GRAVEL, trace of silt (Stratum 5) Very dense micaceous coarse to fine SAND and gravel-sized rock fragments (Decomposed Rock) (Stratum 6)	<u>25.8</u> 25.6	:	8.9			Ν
	on Depth:		(Continue on Sheet 3 of 3) 84.2 ft. Water D	epth:	See	ft., A	fter		hi
Project N			8935.00001		otes				
Project Na Drilling M		Sun	oco Deloach and Short Wharves Repair Mud Rotary			ft., A	fter		_ hr

								Sh	eet 3	A-26
DATE	06	ר <u>דר</u> /1	LOG of BORING No.				See P			01 5
DATE _	00/	2//1	LSURFACE ELEVATION109.8	LOCATI	ON		See r		1	
06 DEPTH, FT.	SAMPLING RESISTANCE	SAMPLE TYPE	DESCRIPTION		STRATUM ELEVATION	POCKET PENETROMETER (TSF)	WATER CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	OTHER TESTS
90- 			Notes: 1. The boring was advanced to approximately 10 using vacuum excavation method (hydro-excavat soils resistance was evaluated using a hand probe were obtained using a hand auger at various dept 2. Unless otherwise indicated, numerical values of "Other Tests" are PID readings from head space jars (in ppm). 3. Drilling resistance (i.e., rig chatter) was encour approximately 36 ft and 41.5 ft depth. 4. Groundwater was measured in the monitoring <u>Date GW Depth (ft) GW Elev (ft)</u> 8/18/2011 9.3 100.5 8/23/2011 9.3 100.5 8/26/2011 9.8 100.0	tion). The e. Samples ths. under of sample ntered at well.						
125										
Comelati	on Donth		84.2 ft.	Motor D	epth:	See	а ^	fter		_ hrs
Project N	on Depth:	1999	<u> 84.2 11. </u>	vvater D		lotes				
-	lo.: lame:		oco Deloach and Short Wharves Repair							
Drilling N			Mud Rotary							



			LOG of BORING No. B-9				Sh		A-27 of 3
DATE	07/	19/11		ON		See Pl			01 0
			SURFACE ELEVATION LOCATI	UN					
DEPTH, FT.	SAMPLING RESISTANCE	SAMPLE TYPE	DESCRIPTION	STRATUM ELEVATION	POCKET PENETROMETER (TSF)	WATER CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	OTHER TESTS
		AU	Dense brown silty coarse to fine SAND and GRAVEL (Fill)						450
5		AU	(Stratum 1)	109.5	_				20
3		AU	Firm to stiff dark gray sandy silty CLAY						400
		AU							340
10	2	AU AU SS				24.3	24	15	420 400 M
	.P.	.P.							
			(Stratum 2)	97.5	_				
	30	SS	Medium dense to dense brown silty SAND and GRAVEL						М
20-			(Stratum 3)	92.5	_				
-			Firm to stiff gray silty CLAY						
25—	8	SS				36.8	46	27	М
	Р	Р			1.5- 1.75	33.7	28	22	M T C
30-	11	SS	- becoming sandy silty CLAY		1.75				
- 35 -	11	SS			0.75- 1.0				М
40	20	SS	(Stratum 4)	72.0	0.75- 1.0				
			Medium dense to dense brown silty coarse to fine SAND	,					
_	18	SS	(Continue on Sheet 2 of 3)			22.6			М
	-	1000		epth:					
Project No Project Na			8935.00001 oco Deloach and Short Wharves Repair	_N	lotes				_ hrs. _ hrs.
Drilling Me		2411	Mud Rotary						



								C 1		A-29
		~ -	10/1	LOG of BORING No. B-9			~ ~			of 3
DATE		07/	19/1	1 SURFACE ELEVATION114.0 LOCAT	ION					
	SAMPLES	SAMPLING RESISTANCE	SAMPLE TYPE	DESCRIPTION	STRATUM ELEVATION	POCKET ETROMET (TSF)	WATER CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	OTHER TESTS
90-	_	100/4"	55	Very dense micaceous brown coarse to fine sand and gravel-sized rock fragments. (Decomposed Rock)	21.0		5.7			М
95-	-	50/1" NQ 52	SS NQ	Medium hard to soft, coarse-grained, moderately to highly weathered Mica Schist, laminations approximately 30 degrees from horizontal, fractures along laminations	114.0 LOCATION See P N With the second			RQE 13		
100-	-				13.9	-				
105-	-			Notes: 1. The boring was advanced to approximately 10 ft depth using vacuum excavation method (hydro-excavation). The soils resistance was evaluated using a hand probe. Samples						
110-				 were obtained using a hand auger at various depths. 2. Unless otherwise indicated, numerical values under "Other Tests" are PID readings from head space of sample jars (in ppm). 3. Groundwater was measured in the monitoring well. 						
115-	-			8/12/201110.5103.58/18/201110.3103.78/23/201110.7103.3						
120-	-									
125-										
130-										
Comp	letio	n Depth:		98.1 ft Water D) epth: (See	ft A	fter		hrs.
Projec			1999	8935.00001	-					
•		ame:		oco Deloach and Short Wharves Repair						_ hrs.
Drilling	g Me	ethod: _		Mud Rotary			ft., A	fter		_ hrs.



Appendix B Laboratory Testing Physical property tests were conducted in the laboratory on selected representative soil samples to aid in classification and for correlation with engineering behavior of the soils. These tests included natural water content (ASTM D 2216), liquid and plastic limits (ASTM D 4318), grain size distribution (ASTM D 422). Three unconsolidated-undrained (UU) triaxial compression tests (ASTM D 2850) and two consolidation tests (ASTM D 2435) were performed on relatively undisturbed Shelby tube samples. One sample was tested for corrosivity evaluation, including pH, resistivity, chlorides, and sulfates.

The numerical results are summarized on Pages B-2 and B-3 and are also shown on the appropriate boring logs. Grain size distribution curves are shown on Pages B-4 through B-14. UU triaxial test results are presented on Pages B-15 through B-17, and consolidation test results on Pages B-18 and B-19.

Project: Sunoco: Deloach and Short Wharves Project No.: 19998935

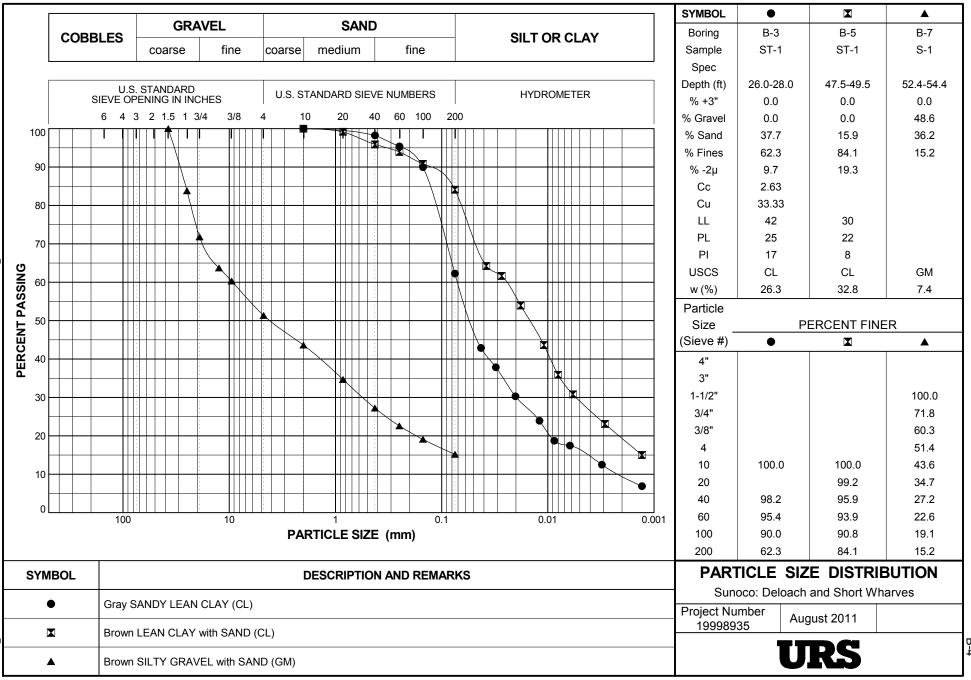
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Boring						Atterberg Limits		<u>г</u>		Grain	on	ation	Analyt	lytical Results		Triaxial Compression		<u> </u>		
Boring nd Sample Number	Depth (feet)	Classification	USCS Symbol	Water Content (%)	Dry Unit Weight (pcf)	Liquid Limit	Plastic Limit	Specific C	Organic Content (%)	<#200 (%)	<2µ (%)	Compaction	Consolidatior	Chloride	(ppm) Sulfate	Sulfide	UU	UC	Resistivity (Ohm-cm)	pН
-3 ST-1	26.0-28.0	Gray SANDY LEAN CLAY	CL	26.3		42	25			62	10	0	0						щÇ	
-3 ST-1	26.0-28.0			31.1	90.9								*							
-3 ST-1	26.0-28.0			27.3	98.1												*			
-5 ST-1	47.5-49.5	Brown LEAN CLAY with SAND	CL	32.8	88.0	30	22			84	19						*			
-7 S-1	52.4-54.4	Brown SILTY GRAVEL with SAND	GM	7.4						15										
-7 S-2	54.4-56.4	Brown SILTY SAND with GRAVEL	SM	11.2						21										
9-7 S-4	58.1-60.1	Gray POORLY GRADED SAND with SILT	SP-SM	11.8						6										
-7 S-5	60.2-62.2	Gray POORLY GRADED SAND	SP	15.6						5										
-7 S-6	62.2-64.2	Gray POORLY GRADED SAND with GRAVEL	SP	10.5						5										
-7 S-7A	67.5-68.5	Gray FAT CLAY	СН	39.0		62	25			97										
-7 S-7B	68.5-69.5	Gray POORLY GRADED SAND with SILT	SP-SM	15.4						5										
-7 S-8	72.5-74.5	Gray POORLY GRADED SAND with SILT and GRAVEL	SP-SM	12.2						8										
-7 S-9	77.5-79.5	Gray CLAYEY SAND	SC	27.8		53	20			35										
5-7 S-10A	82.5-83.5	Gray POORLY GRADED SAND with SILT and GRAVEL	SP-SM	11.7						5										
-7 S-10B	83.5-84.5	Gray WELL-GRADED SAND	SW	10.3						4										
3-8 S-1&S-2	10.0-14.0			20.8	106.7									ND	ND	ND			8200	7.8
-8 S-1&S-2	10.0-16.0	Brown gray SILTY SAND	SM	24.0						19										
-8 S-4	24.0-26.0	Brown gray SILTY SAND	SM	27.8						29										
-8 S-8	39.0-41.0	Gray WELL-GRADED GRAVEL with SAND	GW	14.1						0										
Note: The	soil classifica	ation is based partially on visual classificat	tion unless	both gra	ain size a	nd Atterb	erg limits	are perf	ormed.										Sheet	1 of

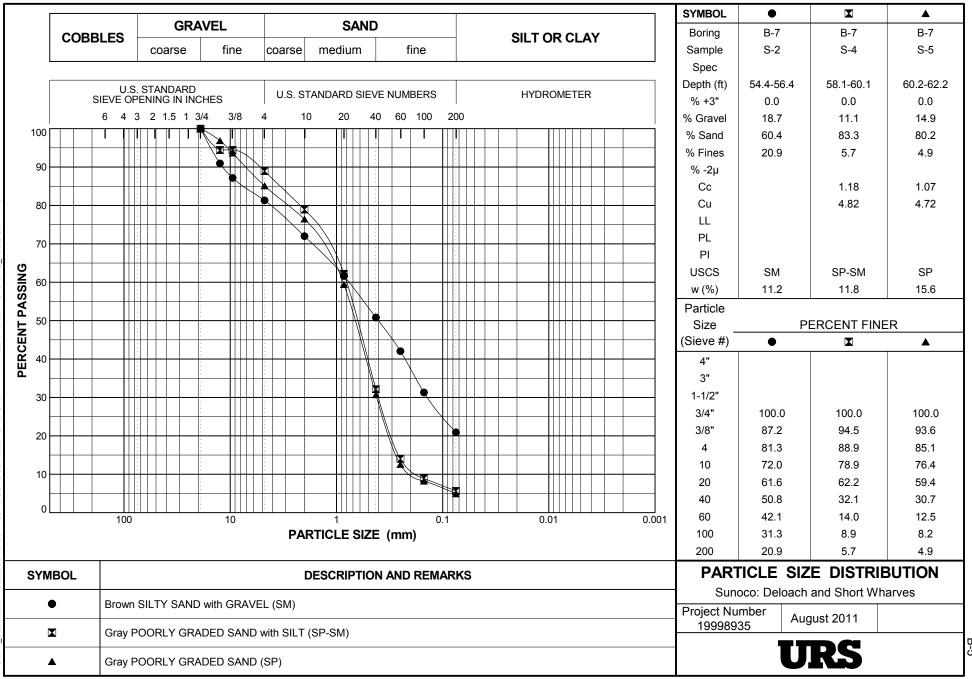
Project: Sunoco: Deloach and Short Wharves Project No.: 19998935

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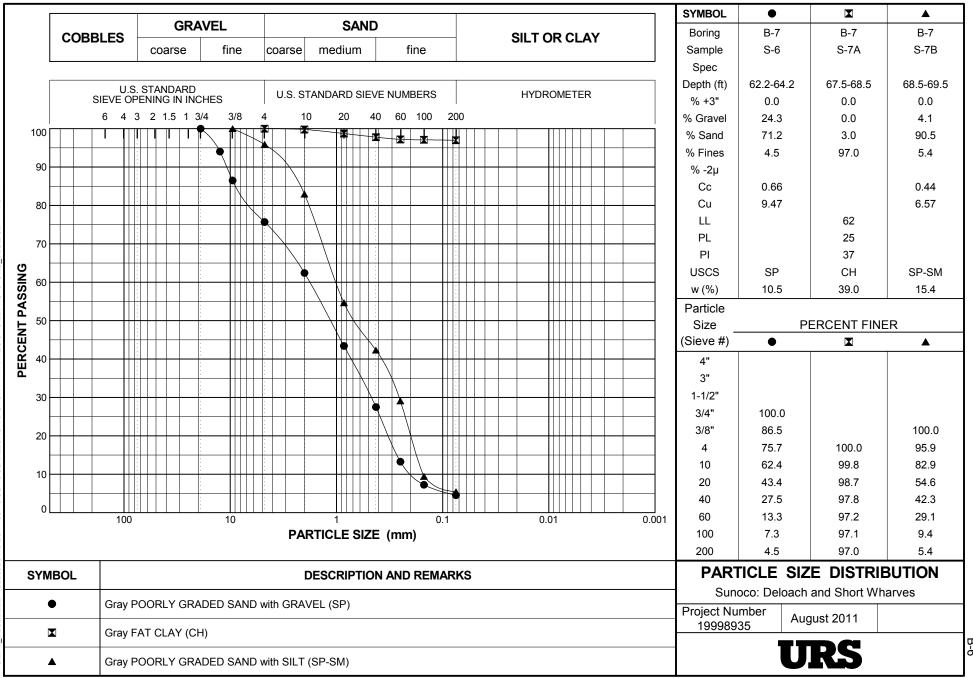
Boring							rg Limits			Grain Size			ation	Analy	lytical Results		Triaxial Compression			
Boring and Sample Number	d Sample Depth	Classification	USCS Symbol	Water Content (%)	Dry Unit Weight (pcf)	Liquid Limit	Plastic Limit	Specific Gravity	Organic cific Content vity (%)	<#200 (%)	<2µ (%)	Compaction	Consolidatior	Chloride	(ppm)		UU	UC	Resistivity (Ohm-cm) d	pН
3-8 S-9	44.0-46.0	Brown SANDY SILT	ML	32.7		37	25			51			0							
3-8 S-12	59.0-61.0	Gray POORLY GRADED GRAVEL with SAND	GP	8.2						2										
3-8 S-15/	73.0-73.3	Gray FAT CLAY	СН	43.7		61	26			100										
3-8 S-15E	73.3-73.8	Gray POORLY GRADED SAND with SILT and GRAVEL	SP-SM	8.5		NP	NP			5										
3-8 S-150	73.8-74.2	Gray FAT CLAY	СН	37.4		66	26			96										
3-8 S-17/	83.0-85.0	Gray POORLY GRADED SAND with GRAVEL	SP	8.9						4										
3-9 S-′	11-13	Brown gray LEAN CLAY with SAND	CL	24.3		24	15			75										
3-9 S-2	17-19.5	Brown SILTY SAND with GRAVEL	SM	8.9						14										
3-9 S-:	23.4-25.4	Gray LEAN CLAY	CL	36.8		46	27			96										
3-9 ST-2	26.0-28.0	Gray SILTY CLAY	CL-ML	33.7		28	22			93	14									
3-9 ST-2	26.0-28.0			35.0	86.4								*							
3-9 ST-2	26.0-28.0			26.8	96.8												*			
3-9 S-{	33.5-35.5	Brown SANDY SILTY CLAY	CL-ML	24.2		24	20			56										
B-9 S-7	43.3-45.3	Brown WELL-GRADED SAND with SILT	SW-SM	22.6						11										
3-9 S-9	53.3-55.3	Brown WELL-GRADED GRAVEL with SAND	GW	8.6						3										
B-9 S-1 ⁻	63.5-65.5	Brown POORLY GRADED GRAVEL	GP	3.6						0										
B-9 S-12	68.5-70.5	Gray FAT CLAY	СН	35.6		56	20			100										
3-9 S-14	78.5-80.5	Gray POORLY GRADED GRAVEL with SILT and SAND	GP-GM	9.1		NP	NP			7										
3-9 S-16	89-91	Gray WELL-GRADED GRAVEL with SAND	GW	5.7						4										
Note: The	soil classific	ation is based partially on visual classification	on unless	both gra	ain size a	nd Atterb	erg limits	are perf	ormed.			•				·			I	



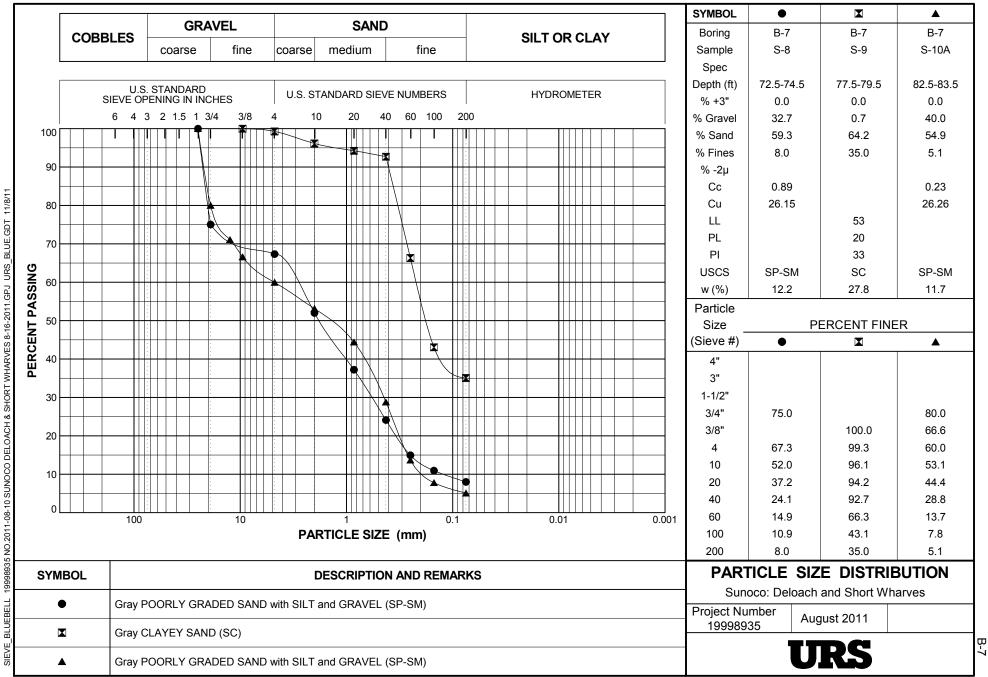
B-4

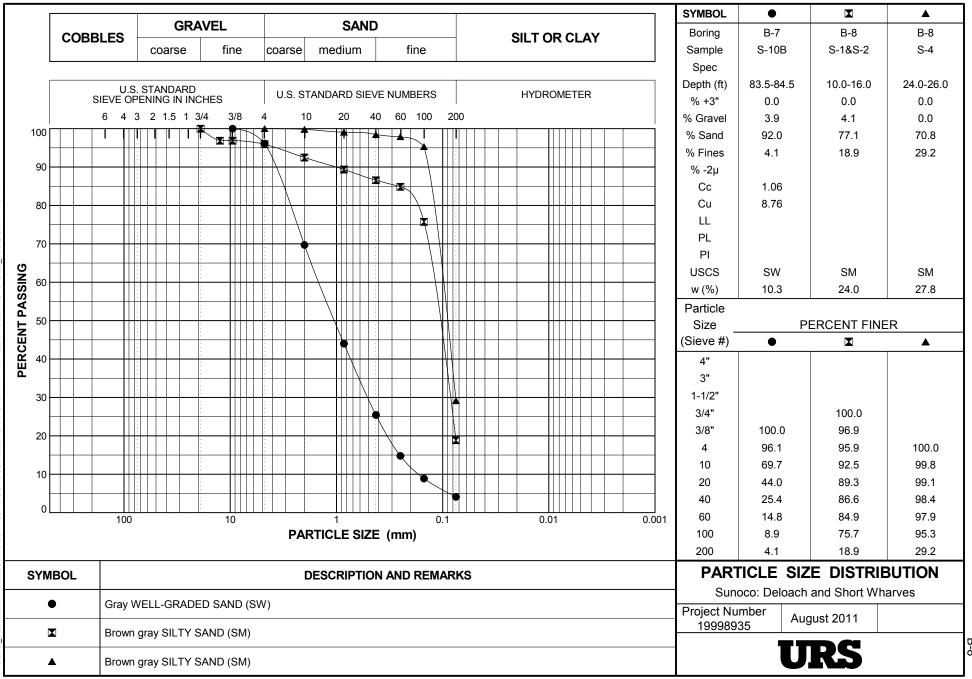


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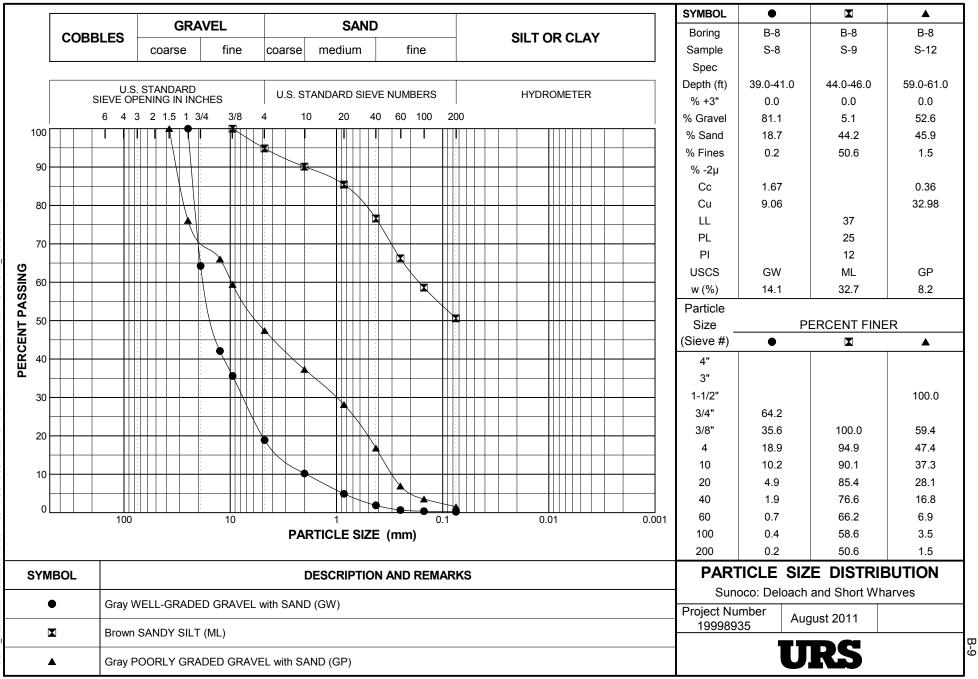


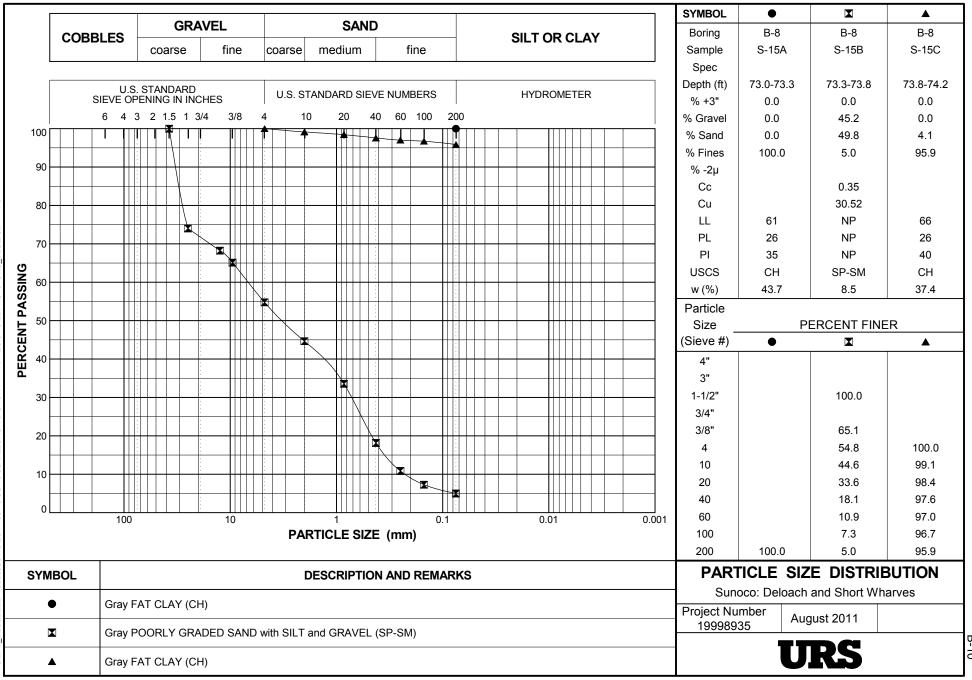
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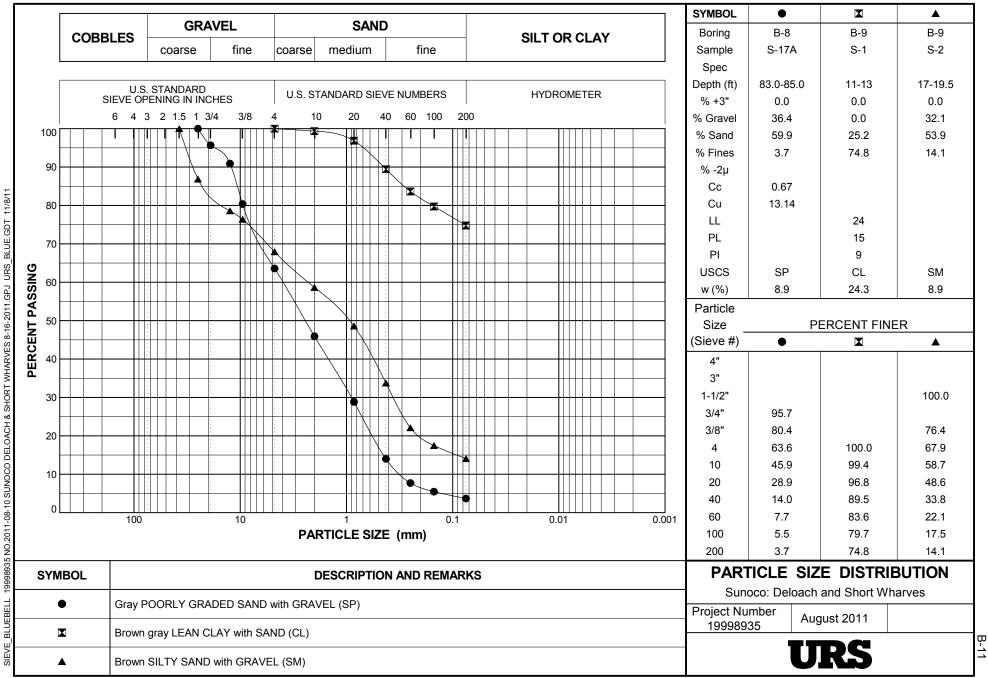


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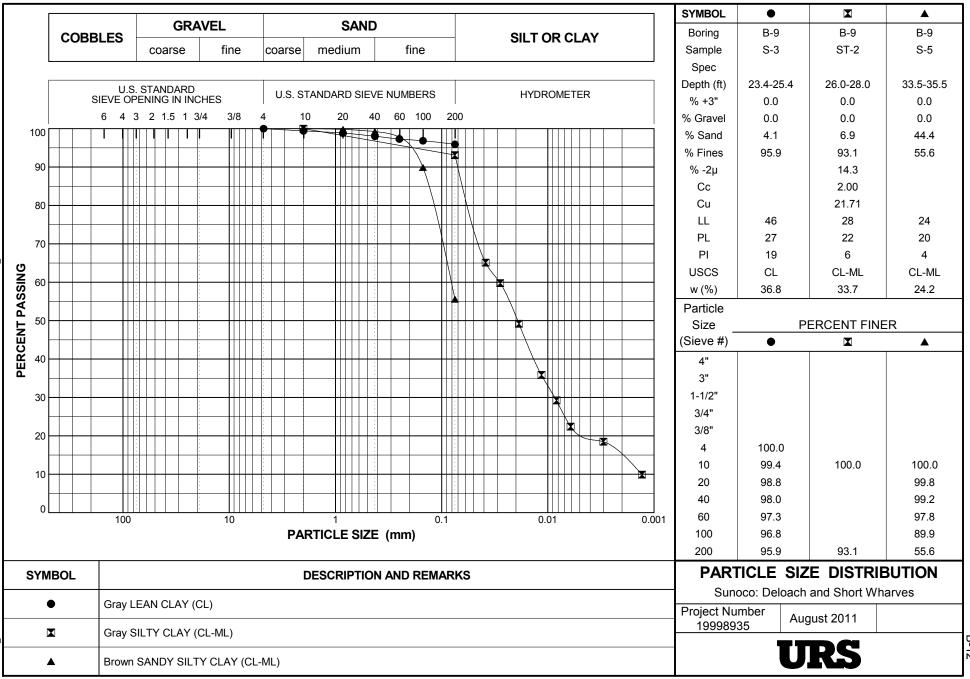




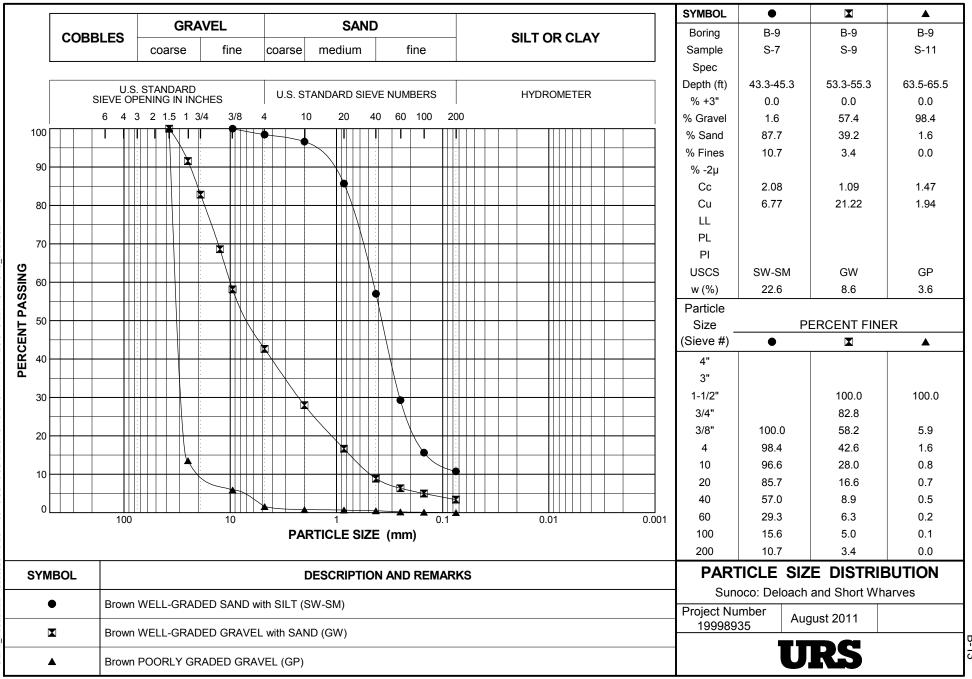
B-10



19998935 NO.2011-08-10 SUNOCO DELOACH & SHORT WHARVES 8-16-2011.GPJ $\,$ URS_ BLUEBELL SIEVE



B-12



Р-13

